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SYSTEM IDENTIFICATION BY ARMA MODELING

by

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September 1988

Thesis Advisor

Murali Tummala

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SYSTEM IDENTIFICATION BY ARMA MODELING

by

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requirements for the degree of

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ABSTRACT

System identification concerns the mathematical modeling of a system based upon its input and output. It allows the development of a mathematical description when all that is available is the result of a process or the output of a system and not the process or system itself.

The purpose of this thesis is to develop algorithms for modeling systems as autoregressive-moving-average processes using the method of instrumental variables, a modification of the ordinary least-squares technique, and a multichannel method based upon processing the input and output data by separate infinite-impulse-response filters. The methods developed are tested by computer simulation using several second and third-order test cases and the results are presented.



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I. INTRODUCTION

A. SYSTEM IDENTIFICATION BASICS

System identification concerns the modeling of systems as sets of mathematical equations based upon the input and output of the system. [Ref. 1: pp. 3-6]. It allows a model to be developed when all that is available is the result of a process or the output of a system and not the process or the system itself. System identification is an important area of study. Solution of the modeling problem offers many alternatives for the continued study of the system. Among these are:

- Nondestructive analysis of the system.
- Simulation studies using the model.
- Easy adaptation of the model to changing system environment.
- Spectral analysis of the system.

Modeling can simulate the system's operation at a fraction of the cost of actual system operation. Complex operations not possible with the actual system for fear of damaging it or personal injury can be simulated. This can expose how the system will operate in adverse conditions not normally experienced. In speech processing, modeling the speech process has the potential for significantly reducing the amount of information necessary to store in order to reproduce the speech.

The modeling process shown in Figure 1 on page 2 assumes the unknown system's input and the output data are available for processing. In many cases, if the system's input is unknown or data is not available, a white noise input can be used in its place. The modeling process uses the input and output data to find a set of parameters which closely approximate the operation of the system. The better the identification technique, the more closely the model follows the performance of the actual system.

Many types of models are available. This thesis investigates a linear parametric model that can be described by difference equations. This type of model lends itself well to simulation on a digital computer. The frequency characteristics of the system determined from the parameters of these types of models are more accurate than what can be determined from classical means such as FFTs. This is because classical methods use windows which assume data beyond their extent is zero [Ref. 2: p. 173]. This is not a realistic assumption. Models in this category include the moving-average (MA) model,

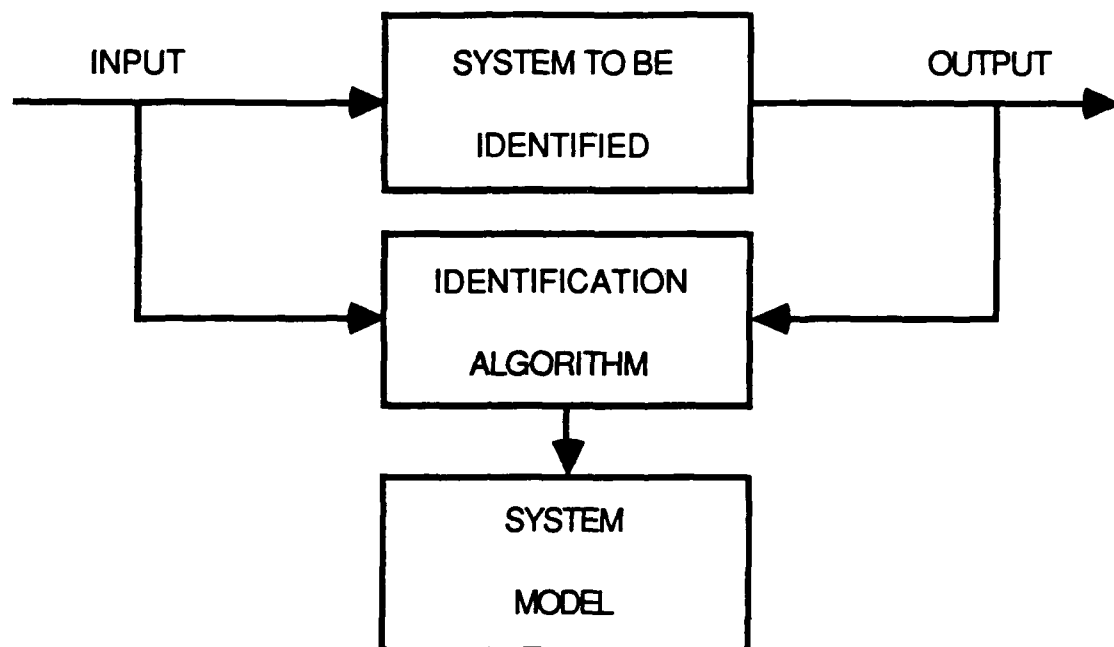


Figure 1. System identification problem

the autoregressive (AR) model, and the autoregressive-moving-average (ARMA) model. In the frequency domain, MA processes are characterized by sharp nulls and smooth peaks and AR processes are characterized by smooth nulls and sharp peaks. ARMA processes have sharp peaks and sharp nulls [Ref. 2: p. 173]. An advantage of the MA process is its inherent stability. An advantage of the AR process is the large number of algorithms already available for modeling systems. An advantage of the ARMA process is that it uses far fewer parameters than either the MA or AR process alone to model a system. This satisfies the general requirement to reduce the complexity of the model.

In addition to a large variety of models, there are two processing modes: block and sequential.

Block processing uses a fixed length block of data in the parameter estimation process. It ignores data before and after the block. This is not a real time processing method because all data must be available before processing can start. Block processing generally involves inversions of data matrices whose sizes are on the order of $(N + M) \times (N + M)$ where N is the order of the AR process and M is the order of the MA process.

Sequential processing uses new data to update the parameter estimations. It starts by initializing an estimate of the inverse of the data covariance as a diagonal matrix. It uses each new data point to update this matrix. Then it updates the parameter estimates using the updated inverse data covariance matrix. It is a real time method. The algorithm to implement the sequential processing method is generally more complex than the block method but less computationally intensive because the matrix inversions are not required.

This thesis concerns only systems represented by discrete time data uniformly sampled at a sufficient rate to meet the Nyquist criteria.

The work in this thesis assumes that the input data is a wide-sense stationary random sequence. Tests of the algorithms used a pseudorandom Gaussian input with a mean of zero and a variance of one.

B. PROBLEM STATEMENT

The purpose of this thesis is to develop algorithms for modeling systems as ARMA processes using the method of instrumental variables (IV) and a multichannel approach. Tests of the methods will be conducted to determine the accuracy of their results and the speed with which they converge.

The IV approach is a modification of the method of ordinary least squares. This approach is developed first as a block processing case and then converted to a sequential processing case. Tests are conducted of only the sequential processing case.

Using a multichannel scheme allows the input and output data of the unknown system to be processed separately. This reduces the sizes of the data matrices involved in the modeling process. Both block and sequential processing cases are formulated but only the block processing case is tested.

C. OVERVIEW OF THESIS

Chapter 2 is about ARMA modeling. It also presents a detailed derivation of the method of ordinary least squares because it forms the basis on which other modeling techniques depend.

Chapter 3 presents a modified least-squares approach called the method of instrumental variables. It is attractive due to its simplicity and good noise performance. Chapter 3 presents results of using this method on several second and third-order test systems.

Chapter 4 presents a new multichannel approach to ARMA modeling. This approach is presented in block and sequential processing forms. This chapter also presents several adaptations of the block form which improve its speed of convergence.

Chapter 5 contains a summary of the thesis and lists topics for further research.

The appendix contains the programs used to test the sequential IV algorithm and the block multichannel iterative algorithm. Subroutines common to both programs are grouped together and listed at the end of the appendix.

II. ARMA MODELING

A. ARMA PROCESSES

Modeling as an autoregressive-moving-average (ARMA) process has the potential for achieving a close fit to the system using a reduced order over that which a moving average or an autoregressive model alone could achieve. ARMA modeling is concerned with finding a set of AR parameters and MA parameters which combined describe an ARMA process that approximates the characteristics of a target system.

The general form of the ARMA model is shown in Figure 2 on page 6. The output at time n , $y(n)$, is a linear combination of past outputs and past and present inputs. The a_i and b_i are constants referred to as tap weights. The a_i parameters form the MA part of the ARMA model. The b_i parameters form the AR part. In equation form the output of the ARMA system is represented by the following difference equation:

$$y(n) = - \sum_{i=1}^N b_i y(n-i) + \sum_{i=0}^M a_i u(n-i) \quad (2.1)$$

where N is the order of the AR part of the ARMA model and M is the order of the MA part of the ARMA model. This means the ARMA output at the current time depends on the last N values of the ARMA output. The N b_i weighting parameters determine exactly how the new output depends on the past outputs. The M a_i weighting parameters determine how the new output depends on the current and $M-1$ past inputs.

Equation (2.1) in vector form becomes:

$$y = \mathbf{x}^T \boldsymbol{\theta} \quad (2.2)$$

where \mathbf{x} is a $(N+M+1) \times 1$ vector of input and output data values given by:

$$\mathbf{x} = [-y(n-1) \quad -y(n-2) \quad \dots \quad -y(n-N) \quad x(n) \quad x(n-1) \quad \dots \quad x(n-M)]^T \quad (2.3)$$

and $\boldsymbol{\theta}$ is a $(N+M+1) \times 1$ vector of the AR and MA tap weights given by:

$$\boldsymbol{\theta} = [b_1 \quad b_2 \quad \dots \quad b_N \quad a_0 \quad a_1 \quad \dots \quad a_M]^T \quad (2.4)$$

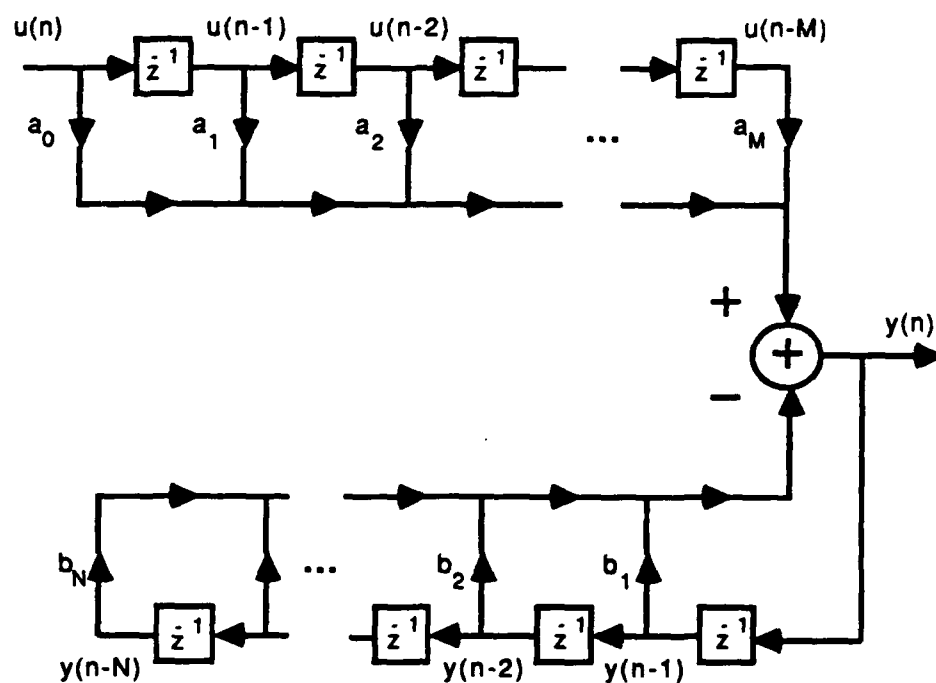


Figure 2. Structure of the ARMA model

For $N + L - 1$ data points available for y and $M + L$ data points available for u , we can write a block equation which gives the value of the output at progressive sampling times:

$$\begin{bmatrix} y(n-L+1) \\ y(n-L+2) \\ \cdot \\ \cdot \\ \cdot \\ y(n) \end{bmatrix} = \begin{bmatrix} x^T(n+1) \\ x^T(n+2) \\ \cdot \\ \cdot \\ \cdot \\ x^T(n+L) \end{bmatrix} \begin{bmatrix} b_1 \\ b_2 \\ \cdot \\ \cdot \\ b_N \\ a_0 \\ a_1 \\ \cdot \\ \cdot \\ a_M \end{bmatrix} \quad (2.5)$$

The i^{th} row in equation (2.5) is the value of y at time $n+i$ based on output data available through time $n+i-1$ and input data available through $n+i$. The i^{th} row is identically equation (2.2) at time $n+i$. In vector form equation (2.5) becomes:

$$y = X\theta \quad (2.6)$$

where θ is defined in equation (2.4); y , the vector of output values, is given by:

$$y = [y(n-L+1) \ y(n-L+2) \ \dots \ y(n)]^T \quad (2.7)$$

and X is a partitioned matrix with rows comprised of data vectors exactly like equation (2.3) only shifted in time. At successive sampling times, when new data is obtained, data used to calculate the previous output shifts one column to the right. The new data fills in the left most y and u columns. The matrix X is given by:

$$X = \begin{bmatrix} -y(n-L) & \dots & -y(n-\eta+1) & u(n-L+1) & \dots & u(n-\mu+1) \\ -y(n-L+1) & \dots & -y(n-\eta+2) & u(n-L+2) & \dots & u(n-\mu+2) \\ \cdot & \dots & \cdot & \cdot & \dots & \cdot \\ \cdot & \dots & \cdot & \cdot & \dots & \cdot \\ \cdot & \dots & \cdot & \cdot & \dots & \cdot \\ -y(n-1) & \dots & -y(n-N) & u(n) & \dots & u(n-M) \end{bmatrix} \quad (2.8)$$

where η is defined as $N+L$ and μ is defined as $M+L$.

If the a_i and b_i are estimates of the true values of the AR and MA parameters, then the filter output will be an estimate of the true output. We use a hat over a variable (for example, \hat{y}) to indicate an estimated value. Rewriting equation (2.6) using the estimated ARMA parameters results in:

$$\hat{y} = X\hat{\theta} \quad (2.9)$$

where $\hat{\theta}$ is defined as:

$$\hat{\theta} = [\hat{b}_1 \ \hat{b}_2 \ \dots \ \hat{b}_N \ \hat{a}_0 \ \hat{a}_1 \ \dots \ \hat{a}_M]^T \quad (2.10)$$

and \hat{y} is now the vector of estimated output values and is given by:

$$\hat{y} = [\hat{y}(n-L+1) \ \hat{y}(n-L+2) \ \dots \ \hat{y}(n)]^T \quad (2.11)$$

Up until now, we have discussed estimating the output of a system given its input, past output, and an estimate of the parameters which describe it. If, however, we know the output and input of the system, based on these equations, we can use them to generate a set of \hat{a}_i and \hat{b}_i which produces an ARMA output which is the best possible estimate of the system output. Then the \hat{a}_i and \hat{b}_i will be optimal parameters for describing the operation of the unknown system as an ARMA process.

B. METHOD OF ORDINARY LEAST-SQUARES

In this thesis we use the method of ordinary least-squares as the means of finding the optimum set of ARMA parameters. It is a well known modeling technique. It offers the advantage of being widely used in the scientific community for a variety of modeling problems. It has been applied successfully to a large number of modeling problems with good results and has been successfully applied to classes of problems for which other methods have failed. [Ref. 3: p. 4]

To apply the method of ordinary least-squares to system identification we form the error between the actual system output and the estimated output generated by the ARMA model. This error is given by:

$$\varepsilon = y - \hat{y} = y - X\hat{\theta} \quad (2.12)$$

where y is the vector of the actual system outputs given by equation (2.7) and \hat{y} is the vector of ARMA outputs given by equation (2.11). [Ref. 1: p. 176]

We then let the sum of the squares of the errors at the instances of time the measurements of the data were taken become a measure of how well the estimates approximate the true system outputs. This measure of performance, or cost function, is denoted J . It is written in equation form as:

$$J = \sum_{i=n+1}^{n+L} \varepsilon_i^2 = \varepsilon^T \varepsilon \quad (2.13)$$

Replacing the error in equation (2.13) with its equivalent expression from equation (2.12) results in:

$$J = y^T y + \hat{\theta}^T X X^T \hat{\theta} - 2 \hat{\theta}^T X y \quad (2.14)$$

Equation (2.14) shows that the performance measure is a function of the estimated parameters. The criterion is to minimize the measure of performance by taking its derivative with respect to the parameter estimates and setting it equal to zero. Then equation (2.14) becomes:

$$\frac{\partial J}{\partial \hat{\theta}} = 0 = 0 + 2 X X^T \hat{\theta} - 2 X^T y \quad (2.15)$$

Solving for $\hat{\theta}$, the parameters, gives us the result:

$$\hat{\theta} = (X^T X)^{-1} X^T y \quad (2.16)$$

Equation (2.16) is the ordinary least-squares solution for the optimum ARMA parameters. It provides the best possible description, in a least-squares sense, of the data source. The resulting parameters provide the closest fit to the actual input and output data of the system in the sense of least-squares errors.

Equation (2.16) uses a block processing approach. The product of $X^T X$ must be formed and then inverted in order to calculate $\hat{\theta}$. In addition to being computationally intensive, the estimate cannot be updated when new data becomes available without recalculating $(X^T X)^{-1}$. A sequential update which does not require $(X^T X)^{-1}$ to be recalculated is presented in the next chapter in the context of the instrumental variable method of least-squares.

III. INSTRUMENTAL VARIABLE METHOD OF SYSTEM IDENTIFICATION

A. INTRODUCTION

The instrumental variable (IV) method of system identification is a variation of the method of ordinary least-squares. Its attraction over ordinary least-squares is that there is no bias in estimating the parameters when dealing with noise [Ref. 4: p. 406]. Also, this method is known to yield consistent estimates and remains as easy to use as the method of ordinary least-squares [Ref. 3: p. 119].

When an additive noise term is present in the observable output, $y(n)$, the output is given by:

$$y(n) = w(n) + v(n) \quad (3.1)$$

Here $w(n)$ represents the actual output of the system and $v(n)$ represents the noise. When this noise has a non-zero mean, using the noise corrupted output to model the unknown system by the ordinary least-squares approach leads to inaccurate estimates of its parameters. The parameters are referred to as biased estimates. [Ref. 3: p. 119, Ref. 1: pp. 192-193, and Ref. 5: p. 704].

The IV method shown in Figure 3 on page 11 generates an estimate of the unknown system's output by processing the input data through an auxiliary model which closely approximates the unknown system. In our implementation of the IV method, the auxiliary model is an ARMA model. Its output is free of the noise affecting the unknown system. The IV method uses the auxiliary model output (estimate), \hat{w} , to calculate the parameters of the unknown system. Therefore the IV parameter estimates are not biased like those generated by the method of ordinary least-squares.

The IV method assumes the existence of a matrix Z composed of the auxiliary model's input and output data which has the following two properties [Ref. 4: p. 406]:

$$\lim_{N \rightarrow \infty} \frac{1}{N} Z^T \varepsilon = 0 \quad (3.2)$$

$$\lim_{N \rightarrow \infty} \frac{1}{N} Z^T X = Q \quad (3.3)$$

where ε is the error in fitting the parameter estimates to the data and is given by:

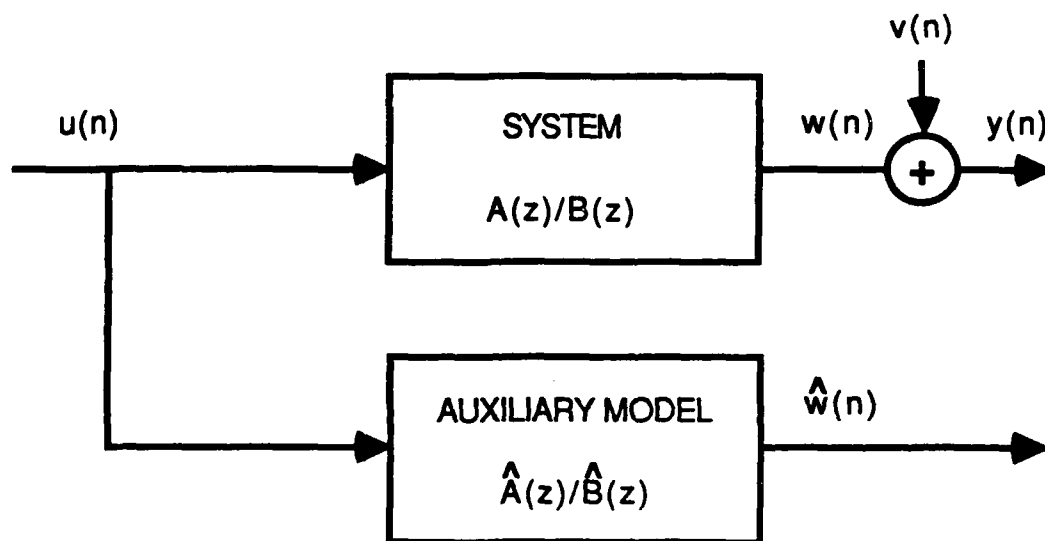


Figure 3. Modeling by the instrumental variable method

$$\varepsilon = y - X\hat{\theta}_{IV} \quad (3.4)$$

and Q is a nonsingular square matrix.

The first property means Z is orthogonal to the error. This leads to the cancellation of the bias term inherent in ordinary least-squares techniques [Ref. 4: p. 406]. The second property ensures the inverse of $Z^T X$ exists. Z is assumed to have the same structure and size as the data matrix X in equation (2.8). Its contents differ in that the noise corrupted system output $y(n)$ in X is replaced by the output of the auxiliary model $\hat{w}(n)$ in Z . The new data matrix Z is given by:

$$Z = \begin{bmatrix} -\hat{w}(n-L) & \dots & -\hat{w}(n-\eta+1) & u(n-L+1) & \dots & u(n-\mu+1) \\ -\hat{w}(n-L+1) & \dots & -\hat{w}(n-\eta+2) & u(n-L+2) & \dots & u(n-\mu+2) \\ \vdots & \dots & \vdots & \vdots & \dots & \vdots \\ \vdots & \dots & \vdots & \vdots & \dots & \vdots \\ -\hat{w}(n-1) & \dots & -\hat{w}(n-N) & u(n) & \dots & u(n-M) \end{bmatrix} \quad (3.5)$$

where η is defined as $N + L$ and μ is defined as $M + L$. Comparing X in equation (2.8) and Z in equation (3.5), we note the substitution of $\hat{w}(n)$ for $y(n)$. Thus, we are now using estimates of the true output $\hat{w}(n)$ instead of noise corrupted samples $y(n)$.

To incorporate Z into the parameter estimation process we begin with equation (2.12), which we rewrite as:

$$y = X\hat{\theta} + \varepsilon \quad (3.6)$$

This equation says that the estimates of the output, given by $X\hat{\theta}$, differ from the actual outputs, y , by some fitting error ε . Multiplying equation (3.6) by Z^T yields:

$$Z^T y = Z^T X \hat{\theta} + Z^T \varepsilon \quad (3.7)$$

Equation (3.3) ensures that $Z^T X$ can be inverted. Solving for $\hat{\theta}$ results in:

$$\hat{\theta} = (Z^T X)^{-1} Z^T y - (Z^T X)^{-1} Z^T \varepsilon \quad (3.8)$$

The $(Z^T X)^{-1} Z^T y$ term in equation (3.8) is the IV estimate of the parameters. It is written as:

$$\hat{\theta}_{IV} = (Z^T X)^{-1} Z^T y \quad (3.9)$$

The $(Z^T X)^{-1} Z^T \varepsilon$ term in equation (3.8) represents a potential bias in the estimate. The first property of the Z matrix, given in equation (3.2), ensures this bias goes to zero, asymptotically. Applying this property, equation (3.8) can be rewritten as:

$$\hat{\theta} = (Z^T X)^{-1} Z^T y = \hat{\theta}_{IV} \quad (3.10)$$

Equation (3.10) gives an unbiased estimate of the ARMA parameters. [Ref. 1: pp. 192-193]:

Other least-squares methods avoid the bias inherent in ordinary least-squares but they are more complicated than the IV method to implement [Ref. 3: p. 119]. Although this thesis does not attempt an analysis of the IV method in the presence of noise, any practical system identification technique must deal with noise. Hence, the attraction of and the desire to use the IV method.

Equation (3.10) represents the block processing case. It assumes $N + L - 1$ output samples and $M + L$ input samples are available. These samples are used to calculate an

estimate of the parameters. Samples beyond this range are not included in the estimation process. Block processing involves multiplication of two $L \times (N + M + 1)$ matrices to form a third matrix. Then this third matrix must be inverted. This is a computationally intensive process. In what follows, we present a sequential algorithm to compute $\hat{\theta}_{IV}$ which avoids matrix inversions.

B. SEQUENTIAL LEAST-SQUARES ESTIMATION USING INSTRUMENTAL VARIABLES

A sequential process for estimating the parameters of an unknown system requires fewer computations than a block process. In a manner similar to that presented in Hsia [Ref. 3: pp. 22-25] for the general least-squares case, the block IV estimation process described above can be converted into a sequential IV estimation process. Using the sequential process also allows the coefficients to be updated based on the new data that becomes available.

The derivation of the sequential estimation procedure consists of two parts. The first part is the derivation of an equation to update the data matrix, $Q(m+1)$, based on the previous data matrix, $Q(m)$, and the new data: $\hat{w}(m)$, $y(m)$, and $u(m+1)$ where m represents the iteration. The second part involves developing an equation for updating the estimate of the parameters, $\hat{\theta}_{IV}(m+1)$, based on the previous estimate, $\hat{\theta}_{IV}(m)$, the previous data matrix, $Q(m)$, and the new data: $\hat{w}(m)$, $y(m)$, and $u(m+1)$.

Define the data matrix $Q(m)$ to be:

$$Q(m) = [Z_m^T X_m]^{-1} \quad (3.11)$$

where Z_m is given by equation (3.5) and X_m is given by equation (2.8). The property of equation (3.3) assures that Q exists. Note that $Q(m)$ includes output data available through m and input data available through $m+1$. Since both Z_m and X_m are $m \times (N + M)$ matrices, $Q(m)$ will be a $(N + M) \times (N + M)$ matrix. As the number of rows of Z and X increase to accommodate the increasing numbers of data points, the size of Q will remain the same. At the next sample time, i.e., at $m+1$, the data matrix becomes:

$$Q(m+1) = [Z_{m+1}^T X_{m+1}]^{-1} \quad (3.12)$$

where the data matrices at $m+1$ are given by:

$$Z_{m+1} = \begin{bmatrix} Z_m \\ \dots \\ z^T(m+1) \end{bmatrix} \quad (3.13)$$

$$X_{m+1} = \begin{bmatrix} X_m \\ \dots \\ x^T(m+1) \end{bmatrix} \quad (3.14)$$

and $z^T(m+1)$ and $x^T(m+1)$ are vectors which contain the most recent data values. Substituting equations (3.13) and (3.14) into equation (3.12) and expanding, results in:

$$Q(m+1) = \left[\begin{bmatrix} Z_m^T & z(m+1) \end{bmatrix} \begin{bmatrix} X_m \\ \dots \\ x^T(m+1) \end{bmatrix} \right]^{-1} \quad (3.15)$$

Expanding further yields:

$$Q(m+1) = [Z_m^T X_m + z(m+1)x^T(m+1)]^{-1} \quad (3.16)$$

In equation (3.16) we see that two terms make up the new data matrix. The $Z_m^T X_m$ term is all the data that was available through time m . The $z(m+1)x^T(m+1)$ term contains the new data. To perform the inversion, let $A = Z_m^T X_m$, $B = z(m+1)$, $C = 1$ and $D = x^T(m+1)$. Then by the matrix inversion lemma:

$$Q(m+1) = A^{-1} - A^{-1}B(C^{-1} + DA^{-1}B)^{-1}DA^{-1} \quad (3.17)$$

Substituting the appropriate expressions for A , B , C , and D back into equation (3.17) yields the equation:

$$\begin{aligned} Q(m+1) &= (Z_m^T X_m)^{-1} - (Z_m^T X_m)^{-1} z(m+1) \\ &\quad \cdot [1 + x^T(m+1)(Z_m^T X_m)^{-1} z(m+1)]^{-1} \\ &\quad \cdot x^T(m+1)(Z_m^T X_m)^{-1} \end{aligned} \quad (3.18)$$

Substituting $Q(m)$ for $(Z_m^T X_m)^{-1}$ reduces equation (3.18) to:

$$\begin{aligned} Q(m+1) &= Q(m) - Q(m)z(m+1)[1 + x^T(m+1)Q(m)z(m+1)]^{-1} \\ &\quad \cdot x^T(m+1)Q(m) \end{aligned} \quad (3.19)$$

This completes the first step of the derivation. Equation (3.19) expresses Q at time $m + 1$ in terms of the old Q and the new data. The term in the brackets is a scalar. Computational intensity has been reduced because a large matrix does not have to be generated and its inverse does not have to be calculated.

Continuing with the derivation, the estimate $\hat{\theta}_{IV}$ for data available through m can be written as:

$$\hat{\theta}_{IV}(m) = (Z_m^T X_m)^{-1} Z_m^T y_m \quad (3.20)$$

The estimate $\hat{\theta}_{IV}$ for data available through $m + 1$ can be written as:

$$\hat{\theta}_{IV}(m + 1) = (Z_{m+1}^T X_{m+1})^{-1} Z_{m+1}^T y_{m+1} \quad (3.21)$$

Substituting equation (3.12) into equation (3.21) results in an expression for the estimate of the parameters in terms of the new data matrix and all the available data given by:

$$\hat{\theta}_{IV}(m + 1) = Q(m + 1) Z_{m+1}^T y_{m+1} \quad (3.22)$$

$$\hat{\theta}_{IV}(m + 1) = Q(m + 1) [Z_m^T \quad z(m + 1)] \begin{bmatrix} y_m \\ \dots \\ y(m + 1) \end{bmatrix} \quad (3.23)$$

$$\hat{\theta}_{IV}(m + 1) = Q(m + 1) [Z_m^T y_m + z(m + 1) y(m + 1)] \quad (3.24)$$

Substituting for $Q(m + 1)$ from equation (3.19) and expanding results in:

$$\begin{aligned} \hat{\theta}_{IV}(m + 1) &= Q(m) Z_m^T y_m \\ &\quad - Q(m) z(m + 1) [1 + x^T(m + 1) Q(m) z(m + 1)]^{-1} x^T(m + 1) Q(m) Z_m^T y_m \\ &\quad + Q(m) z(m + 1) y(m + 1) \\ &\quad - Q(m) z(m + 1) [1 + x^T(m + 1) Q(m) z(m + 1)]^{-1} \\ &\quad \cdot x^T(m + 1) Q(m) z(m + 1) y(m + 1) \end{aligned} \quad (3.25)$$

Although somewhat lengthy, this equation has the desired form. To simplify it, its last two terms can be arranged into the form:

$$\begin{aligned} &Q(m) z(m + 1) \{1 - [1 + x^T(m + 1) Q(m) z(m + 1)]^{-1} x^T(m + 1) Q(m) z(m + 1)\} \\ &\quad \cdot y(m + 1) \end{aligned} \quad (3.26)$$

The terms within the braces can be thought of as the result of a previous application of the matrix inversion lemma with $A^{-1} = I$, $B = I$, $C^{-1} = I$ and $D = x^T(m+1)Q(m)z(m+1)$. Reversing the lemma results in:

$$Q(m)z(m+1)[1 + x^T(m+1)Q(m)z(m+1)]^{-1}y(m+1) \quad (3.27)$$

Replacing the last two terms in equation (3.25) with this result gives us:

$$\begin{aligned} \hat{\theta}_{IV}(m+1) = & Q(m)Z_m^T y_m - Q(m)z(m+1)[1 + x^T(m+1)Q(m)z(m+1)]^{-1} \\ & \cdot x^T(m+1)Q(m)Z_m^T y_m + Q(m)z(m+1) \\ & \cdot [1 + x^T(m+1)Q(m)z(m+1)]^{-1}y(m+1) \end{aligned} \quad (3.28)$$

Factoring $Q(m)z(m+1)$ and $[1 + x^T(m+1)Q(m)z(m+1)]^{-1}$ from the last two terms reduces equation (3.28) further to:

$$\begin{aligned} \hat{\theta}_{IV}(m+1) = & Q(m)Z_m^T y_m + Q(m)z(m+1)[1 + x^T(m+1)Q(m)z(m+1)]^{-1} \\ & \cdot [y(m+1) - x^T(m+1)Q(m)Z_m^T y_m] \end{aligned} \quad (3.29)$$

Substituting equation (3.11) into equation (3.20) and then equation (3.20) into equation (3.29) yields the final form for the update of the estimate of the parameters:

$$\begin{aligned} \hat{\theta}_{IV}(m+1) = & \hat{\theta}_{IV}(m) + Q(m)z(m+1) \\ & \cdot [1 + x^T(m+1)Q(m)z(m+1)]^{-1}[y(m+1) - x^T(m+1)\hat{\theta}_{IV}(m)] \end{aligned} \quad (3.30)$$

This is the desired result for updating the estimate of the parameters. Note that like equation (3.19), the matrix inversion of equation (3.21) has been reduced to inversion of a scalar. Equation (3.30) describes the update of $\hat{\theta}_{IV}(m+1)$ in terms of the previous estimate of the parameters, $\hat{\theta}_{IV}(m)$, the previous data matrix, $Q(m)$, and the new data: $\hat{w}(m)$, $y(m)$, and $u(m+1)$.

C. TESTING THE SEQUENTIAL INSTRUMENTAL VARIABLE ALGORITHM

Equations (3.19) and (3.30) above comprise the sequential IV algorithm. Several tests of this algorithm were made using second and third-order filters as unknown systems. Tests were run via computer simulation using the filters to generate the output data. A Gaussian random process with zero mean and unit variance was used as the input. The input was produced by IMSL subroutine GGNML. Graphs were created

using DISSPLA. Table 1 on page 17 shows pole and zero locations as well as numerator and denominator parameters for the test filters.

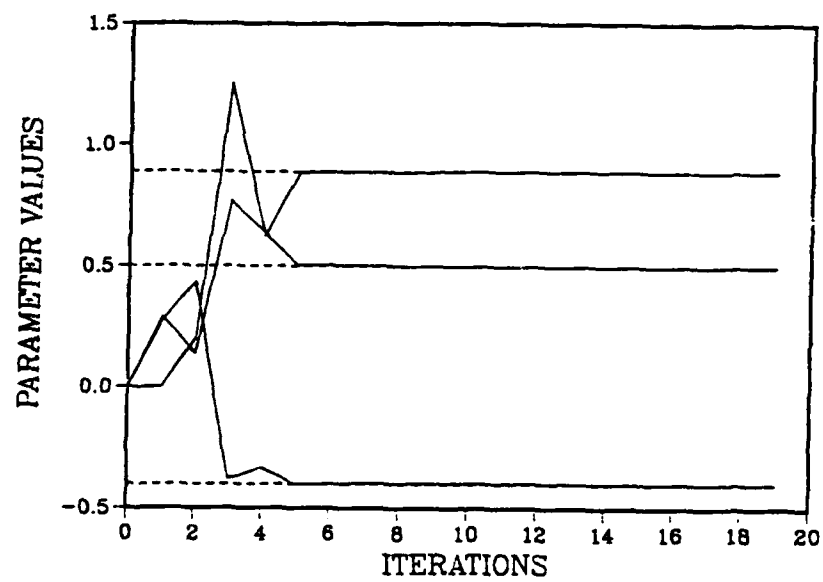
Table 1. TEST SYSTEMS FOR THE IV MODELING METHOD

TEST FILTER	LOCATIONS OF POLES	LOCATIONS OF ZEROS	AR PARAMETERS	MA PARAMETERS
T2	$0.445 + j0.228$ $0.445 - j0.228$	$0.4 + j1.273$ $0.4 - j1.273$	1.0 -0.89 0.25	0.5 -0.4 0.89
T2N	$0.445 + j0.228$ $0.445 - j0.228$	$0.4 + j0.8$ $0.4 - j0.8$	1.0 -0.89 0.25	1.0 -0.80 0.80
T3	0.6605 $0.6647 + j0.502$ $0.6647 - j0.502$	-1.0 -1.0 -1.0	1.0 -1.99 1.57 -0.458	0.0154 0.0462 0.0462 0.0154

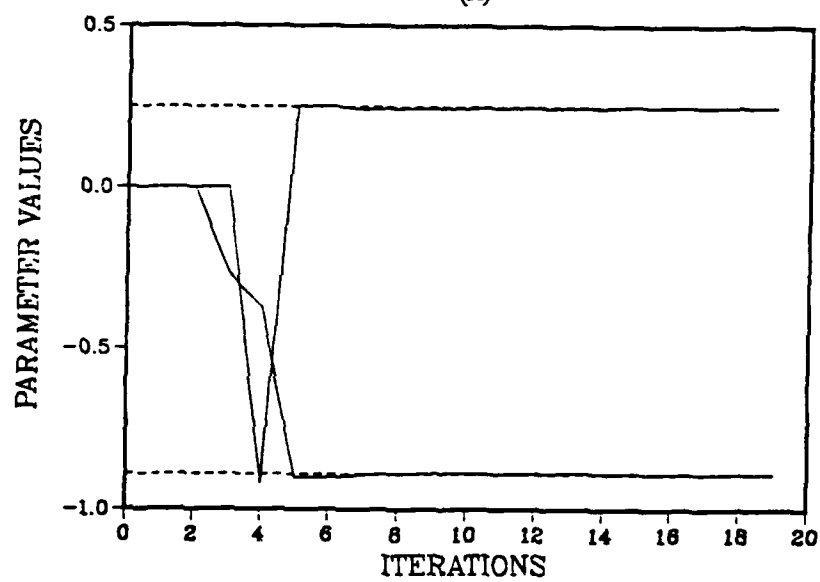
Results of the tests are shown in graphical form in Figure 4 on page 18, Figure 5 on page 19, and Figure 6 on page 20. Dashed lines indicate the true values of the parameters. Solid lines are the IV method's estimates.

For both second-order test cases shown, the algorithm converged quickly and produced accurate results. For the third-order test case, convergence took longer but the values were accurate. A third-order system is more complex than a second-order system, so conceivably it would require more iterations to converge. The number of iterations required is of the same order as the method of ordinary least-squares.

Table 2 on page 21 contains the IV algorithm's best estimates of the parameters and the number of iterations required to converge to those estimates. It also shows the absolute and percent errors from the true parameters.

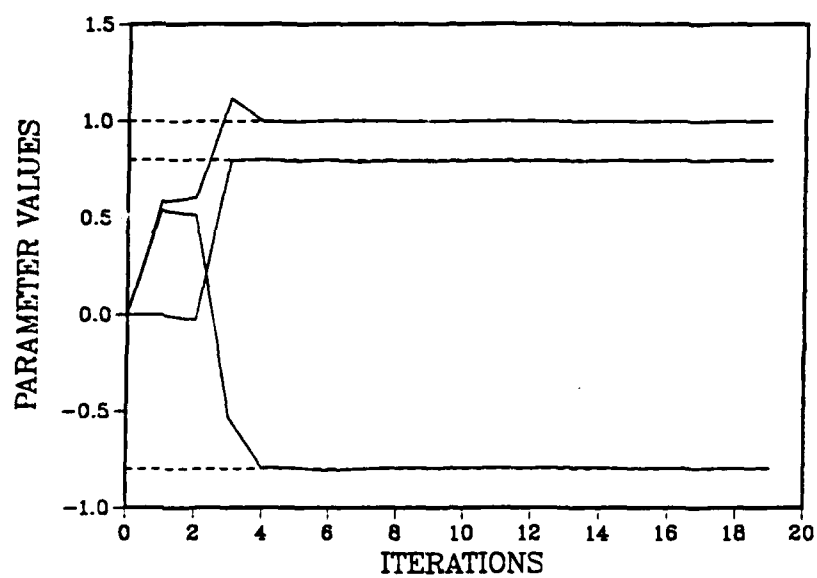


(A)

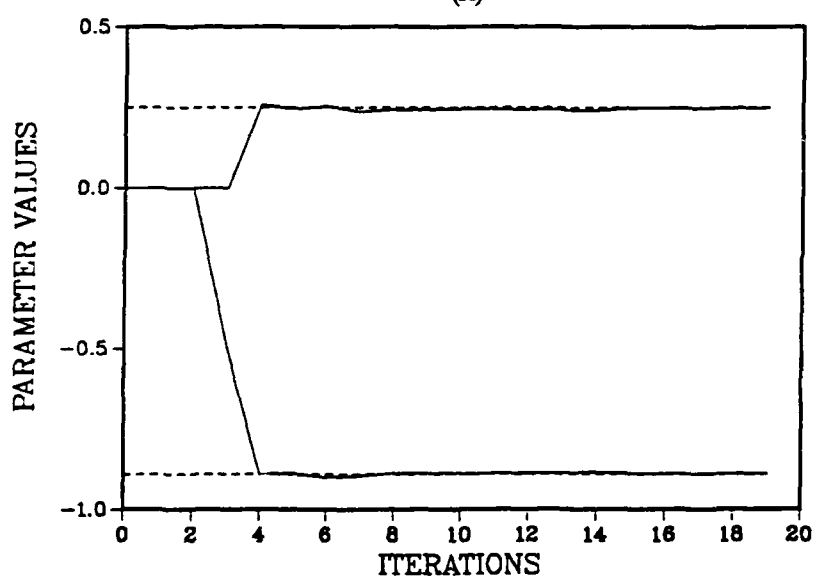


(B)

Figure 4. Second-order test case T2. (A) MA parameters. (B) AR parameters.



(A)



(B)

Figure 5. Second-order test case T2N. (A) MA parameters. (B) AR parameters.

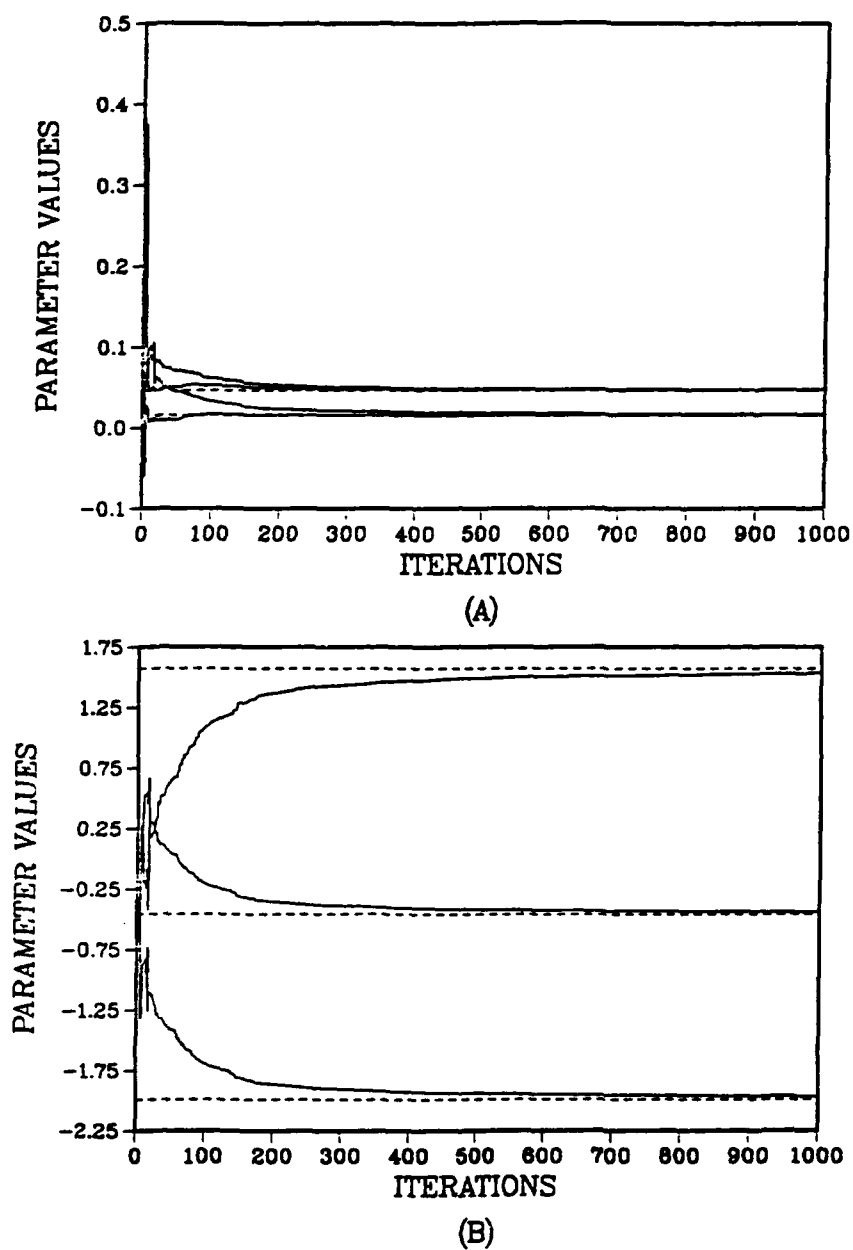


Figure 6. Third-order test case T3. (A) MA parameters. (B) AR parameters.

Table 2. COEFFICIENT ESTIMATES BY THE IV MODELING METHOD.

TEST FILTER	PARAMETER ESTIMATE	ABSOLUTE ERROR	PERCENT ERROR	ITERATIONS
T2	0.500	0.0	0.0	10
	-0.396	+0.004	0.10	
	0.888	-0.002	0.22	
	1.000	0.0	0.0	
	-0.888	+0.002	0.22	
	0.244	-0.006	2.40	
T2N	1.000	0.0	0.0	10
	-0.794	+0.006	0.750	
	0.794	-0.006	0.750	
	1.000	0.0	0.0	
	-0.887	+0.003	0.34	
	0.243	-0.007	2.80	
T3	0.0154	0.0	0.0	1000
	0.0466	+0.0004	0.87	
	0.0475	+0.0013	2.81	
	0.0169	+0.0015	9.74	
	1.000	0.0	0.0	
	-1.96	-0.03	3.0	
	1.532	-0.040	2.01	
	0.4379	-0.0204	4.45	

IV. SYSTEM IDENTIFICATION USING AN ITERATIVE MULTICHANNEL APPROACH

A. INTRODUCTION

This chapter presents an alternate system identification method, the iterative multichannel approach. This approach differs from the IV method and the method of ordinary least-squares presented in the preceding chapters in that it processes the input and output data from the unknown system in separate channels. In its block processing form one advantage over the IV and ordinary least-squares methods is a reduction in the sizes of the data matrices. As a result, the computational complexity of the multichannel algorithm is on the order of $M^2 + N^2$, where M is the order of the MA part and N is the order of the AR part. In contrast, the block IV and ordinary least-squares methods require computations on the order of $(M + N)^2$.

B. PREVIOUS MULTICHANNEL METHODS

Whittle [Ref. 6: pp. 129-130] was the first to develop a multichannel solution for the ARMA modeling problem. He sought to extend the recursive Durbin solution for estimating the parameters of a single variable autoregressive process to a multivariable autoregressive process. He discovered that to do this he would have to fit the data to two autoregressive processes simultaneously. One of the autoregressions would use present data samples to predict the value of the data one time step in the future. This is called forward prediction. The second autoregression would use present data samples to predict the value of the data at the previous time instant and is referred to as backward prediction. Sometime during this research, Whittle determined that if the input was derived from a MA scheme, making the process ARMA, then the solution would remain the same provided the correlations of the input used in the parameter estimation process had shifts greater than the MA scheme. Whittle's use of the two separate and simultaneous autoregressions to model an ARMA process can be thought of as a multichannel modeling approach.

Further work in the area of multichannel ARMA modeling was conducted by Perry and Parker [Ref. 7: pp. 509-510]. They started out with the ARMA problem formulation discussed in Chapter 2. Using the method of ordinary least-squares to minimize the mean square error, they found the solution for the estimate of the parameters to be the Wiener solution given by:

$$\begin{bmatrix} \mathbf{R}_{yy} & \mathbf{R}_{yu'} \\ \mathbf{R}_{u'y} & \mathbf{R}_{u'u'} \end{bmatrix} \begin{bmatrix} \mathbf{b} \\ \mathbf{a}' \end{bmatrix} = \begin{bmatrix} \mathbf{r}_{yy} \\ \mathbf{r}_{yu'} \end{bmatrix} \quad (4.1)$$

In equation (4.1) \mathbf{R}_{yy} is a matrix of autocorrelations of the past outputs, $\mathbf{R}_{u'u'}$ is a matrix of autocorrelations of the inputs, $\mathbf{R}_{yu'}$ and $\mathbf{R}_{u'y}$ are crosscorrelations of the input and output data, \mathbf{b} is a vector of AR parameters, and \mathbf{a}' is a vector of MA parameters. In addition, \mathbf{r}_{yy} is a vector of autocorrelations of past output data with the current output and $\mathbf{r}_{yu'}$ is a vector of crosscorrelations of input data with the current output. By assuming the first MA parameter, a'_0 was known, they were able to treat it as a gain and factor it out of all the other MA parameters. This allowed them [Ref. 7: pp. 509-510] to extract the $(N+1)^{\text{st}}$ row and column of equation (4.1) and rewrite the solution in the form:

$$\begin{bmatrix} \mathbf{R}_{yy} & \mathbf{R}_{yu} \\ \mathbf{R}_{uy} & \mathbf{R}_{uu} \end{bmatrix} \begin{bmatrix} \mathbf{b} \\ \mathbf{a} \end{bmatrix} = \begin{bmatrix} \mathbf{r}_{yy} \\ \mathbf{r}_{yu} \end{bmatrix} - \begin{bmatrix} \mathbf{r}_{yu} \\ \mathbf{r}_{uu} \end{bmatrix} \quad (4.2)$$

In equation (4.2), \mathbf{a}' has been rewritten as \mathbf{a} to indicate that the a'_0 term has been factored out of all of the MA parameters. Reasoning that equation (4.2), the ARMA solution, was a generalization of the AR solution, they figured that it must have a recursive solution consisting of some combination of the Levinson-Durbin algorithm, a recursive solution for the AR problem. They then determined equation (4.2) was in a form similar to Whittle's formulation of the problem. So they reasoned that they could use a form of Whittle's solution to solve the ARMA modeling problem. Like Whittle, their solution consists of a forward and a backward autoregression. It uses two coupled lattice filters to process the input and output data. Off diagonal elements of the lattice coefficient matrices specify the coupling points of the two lattices.

C. ITERATIVE APPROACH TO MULTICHANNEL ARMA MODELING

This thesis proposes another solution to the ARMA modeling problem using the multichannel approach. It is an iterative approach with no direct coupling of the two channels. However, note that there is an implicit coupling in the sense that the ARMA system output samples $y(n)$ are a function of the present and past input samples $u(n)$, and the past output samples. This is shown in equation (2.1). The approach proposed uses two separate finite-impulse-response (FIR) filters to estimate the unknown system. One filter estimates the AR part of the unknown system. The second estimates the MA part of the unknown system. Figure 7 on page 25 shows the structure of this approach.

The derivation of the equations for this approach follows the method of ordinary least-squares.

From Figure 7 on page 25, the value of the signal $Y(z)$ is seen to be $\frac{A(z)}{B(z)} U(z)$. When this signal passes through $C(z)$, if $C(z)$ is close to $B(z)$, the resulting signal $X(z)$ is approximately $A(z)U(z)$. Also from Figure 7 on page 25, the value of $Z(z)$ is seen to be $A(z)U(z)$ provided $D(z)$ is close to $A(z)$. The difference of these two signals forms the error which we seek to minimize by the method of ordinary least-squares. In minimizing the error we seek to drive $D(z)$ and $C(z)$ as close as possible to $A(z)$ and $B(z)$, respectively.

Referring to Figure 7 on page 25, signals $z(n)$ and $x(n)$ are defined as the outputs from two FIR filters and are given by the equations:

$$z(n) = d_0 u(n) + d_1 u(n-1) + d_2 u(n-2) + \dots + d_M u(n-M) = \mathbf{u}^T(n) \mathbf{d} \quad (4.3)$$

$$x(n) = y(n) + c_1 y(n-1) + c_2 y(n-2) + \dots + c_N y(n-N) = \mathbf{y}^T(n) \mathbf{c} \quad (4.4)$$

where the vectors \mathbf{d} and \mathbf{c} represent the systems $D(z)$ and $C(z)$, respectively. The vectors \mathbf{d} , $\mathbf{u}(n)$, \mathbf{c} , and $\mathbf{y}(n)$ are given by the following equations:

$$\mathbf{d} = [d_0 \ d_1 \ d_2 \ \dots \ d_M]^T \quad (4.5)$$

$$\mathbf{u}(n) = [u(n) \ u(n-1) \ u(n-2) \ \dots \ u(n-M)]^T \quad (4.6)$$

$$\mathbf{c} = [1 \ c_1 \ c_2 \ \dots \ c_N]^T \quad (4.7)$$

$$\mathbf{y}(n) = [y(n) \ y(n-1) \ y(n-2) \ \dots \ y(n-N)]^T \quad (4.8)$$

The \mathbf{d} parameters are estimates of the MA portion of the ARMA process. The \mathbf{c} parameters approximate its AR portion. The vector $\mathbf{u}(n)$ is the input data vector of length M , the order of the MA part, and $\mathbf{y}(n)$ is the output data vector equal of length N , the order of the AR part.

Forming the error between x and z results in:

$$e(n) = z(n) - x(n) = \mathbf{u}^T(n) \mathbf{d} - \mathbf{y}^T(n) \mathbf{c} \quad (4.9)$$

The least-squares performance criterion is:

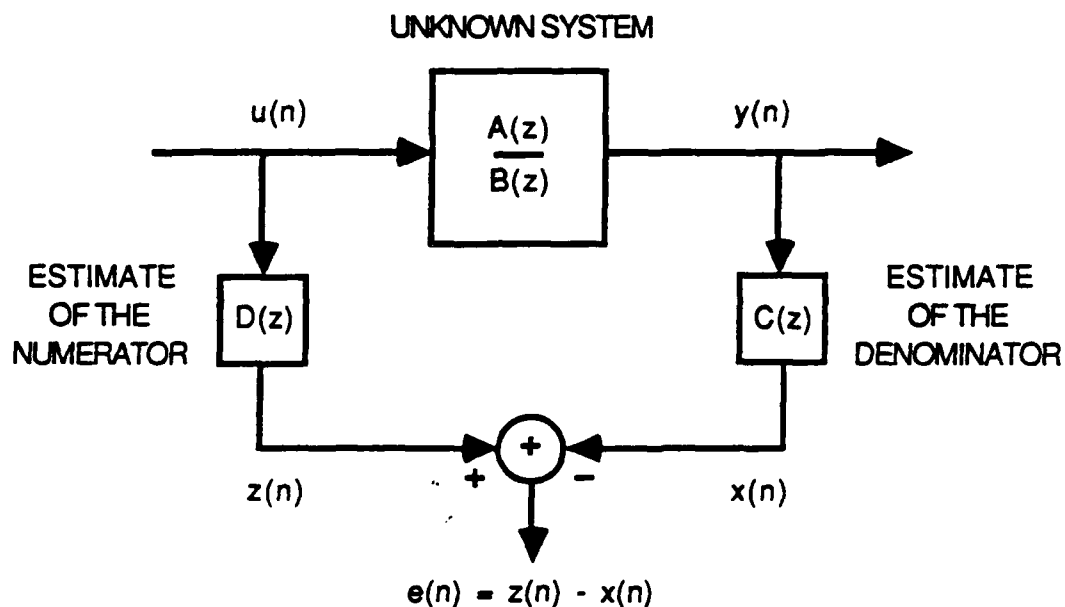


Figure 7. Multichannel modeling process

$$J = \sum_{n=1}^L e^2(n) = \sum_{n=1}^L [z(n) - x(n)]^2 \quad (4.10)$$

Substituting for $e(n)$ from equation (4.9), we can write equation (4.10) in vector form as:

$$J = \sum_{n=1}^L (u^T d - y^T c)^2 \quad (4.11)$$

where we have dropped the time index, n , for convenience. Expanding equation (4.11) results in:

$$J = \sum_{n=1}^L d^T u u^T d + c^T y y^T c - 2d^T u y^T c \quad (4.12)$$

We notice that the performance criterion is a function of both \mathbf{d} and \mathbf{c} . Minimizing the performance criterion by differentiating with respect to the vector \mathbf{c} and equating the results to zero yields:

$$\frac{\partial J}{\partial \mathbf{c}} = 0 = 0 + 2 \sum_{n=1}^L (\mathbf{y}\mathbf{y}^T)\mathbf{c} - 2 \sum_{n=1}^L (\mathbf{y}\mathbf{u}^T)\mathbf{d} \quad (4.13)$$

Similarly, differentiating the performance criterion with respect to the vector \mathbf{d} and equating the result to zero yields:

$$\frac{\partial J}{\partial \mathbf{d}} = 0 = 0 + 2 \sum_{n=1}^L (\mathbf{u}\mathbf{u}^T)\mathbf{d} - 2 \sum_{n=1}^L (\mathbf{u}\mathbf{y}^T)\mathbf{c} \quad (4.14)$$

Solving equation (4.13) for \mathbf{c} and equation (4.14) for \mathbf{d} results in two equations for estimating the AR and MA parameters of the unknown system given by:

$$\mathbf{c} = \mathbf{R}_{yy}^{-1} \mathbf{R}_{yu} \mathbf{d} \quad (4.15)$$

and

$$\mathbf{d} = \mathbf{R}_{uu}^{-1} \mathbf{R}_{uy} \mathbf{c} \quad (4.16)$$

where

$$\mathbf{R}_{uu} = \sum_{n=1}^L \mathbf{u}\mathbf{u}^T = \begin{bmatrix} r_{uu}(0) & r_{uu}(1) & \cdot & \cdot & r_{uu}(N) \\ r_{uu}(1) & r_{uu}(0) & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ r_{uu}(N) & \cdot & \cdot & \cdot & r_{uu}(0) \end{bmatrix} \quad (4.17)$$

is an estimate of the input autocorrelation matrix. The elements of \mathbf{R}_{uu} are computed using the unbiased method as follows:

$$r_{uu}(l) = \frac{1}{L-l} \sum_{j=0}^{L-l} u(j)u(j-l) \text{ for } l=0, 1, 2, \dots, M \quad (4.18)$$

Matrices \mathbf{R}_{yy} , \mathbf{R}_{uy} , and \mathbf{R}_{yu} appearing in equations (4.15) and (4.16) have structures identical to equation (4.17), where \mathbf{R}_{yy} is the estimate of the output autocorrelation matrix, and \mathbf{R}_{uy} and \mathbf{R}_{yu} are estimates of the crosscorrelation matrices. Note that $\mathbf{R}_{yu} = \mathbf{R}_{uy}^T$. The elements of these matrices; r_{yy} , r_{uy} and r_{yu} , are computed as follows:

$$r_{yy}(l) = \frac{1}{L-l} \sum_{j=0}^{L-l} y(j)y(j-l) \text{ for } l = 0, 1, 2, \dots, N \quad (4.19)$$

$$r_{uy}(l) = \frac{1}{L-l} \sum_{j=0}^{L-l} u(j)y(j-l) \text{ for } l = 0, 1, 2, \dots, M \quad (4.20)$$

and

$$r_{yu}(l) = \frac{1}{L-l} \sum_{j=0}^{L-l} y(j)u(j-l) \text{ for } l = 0, 1, 2, \dots, N \quad (4.21)$$

Up to this point, following the standard least-squares procedure has resulted in two dependent or coupled equations to solve for the parameters of an unknown system modeled as an ARMA process. How best to solve these equations? By iteration. The steps of the iterative process are to

- Calculate the correlation matrices and vectors from the available data.
- Initialize \mathbf{c} . Exploit the fact that the first parameter in \mathbf{c} is, $c_0 = 1$.
- Solve for \mathbf{d} from this initial \mathbf{c} .
- Solve for \mathbf{c} from \mathbf{d} .
- Repeat beginning at the third step.

Here is a summary of the equations in proper order for implementing the algorithm:

- Compute \mathbf{R}_{uu} , \mathbf{R}_{yy} and \mathbf{R}_{yu} from equations (4.17) to (4.21). Note that $\mathbf{R}_{yu} = \mathbf{R}_{uy}^T$.
- Initialization:

$$\mathbf{c}^{(0)} = [1 \ 0 \ \dots \ 0]^T \quad (4.22)$$

- For $k = 0$ to K

$$\mathbf{d}^{(k+1)} = \mathbf{R}_{uu}^{-1} \mathbf{R}_{uy} \mathbf{c}^{(k)} \quad (4.23)$$

$$\mathbf{c}^{(k+1)} = \mathbf{R}_{yy}^{-1} \mathbf{R}_{yu} \mathbf{d}^{(k+1)} \quad (4.24)$$

where k is the iteration number.

This is a very simple algorithm. For the case where the AR and MA orders are equal, the correlation matrices are half the size of the block data matrices which must be generated and inverted in the IV algorithm.

1. Testing the Multichannel Iterative Algorithm

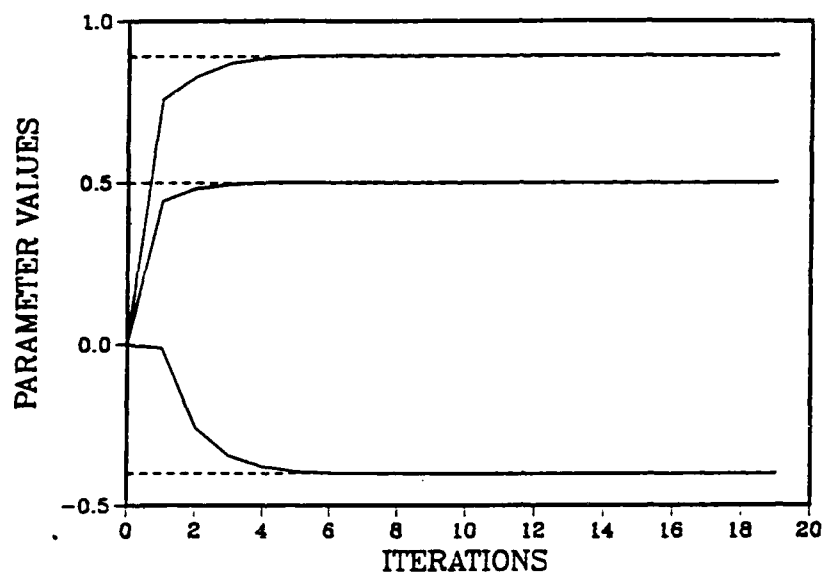
We tested the algorithm by computer simulation using second and third-order filters as unknown systems. Table 3 shows pole and zero locations as well as MA and AR parameters for the test filters. Data lengths of 500 data points were used to calculate the autocorrelation and crosscorrelation matrices. Besides the reported cases, we tested the algorithm on several other second, third and mixed-order cases. The performance of the algorithm in all cases that we tested was fairly uniform.

Table 3. TEST SYSTEMS FOR ITERATIVE MULTICHANNEL MODELING METHOD

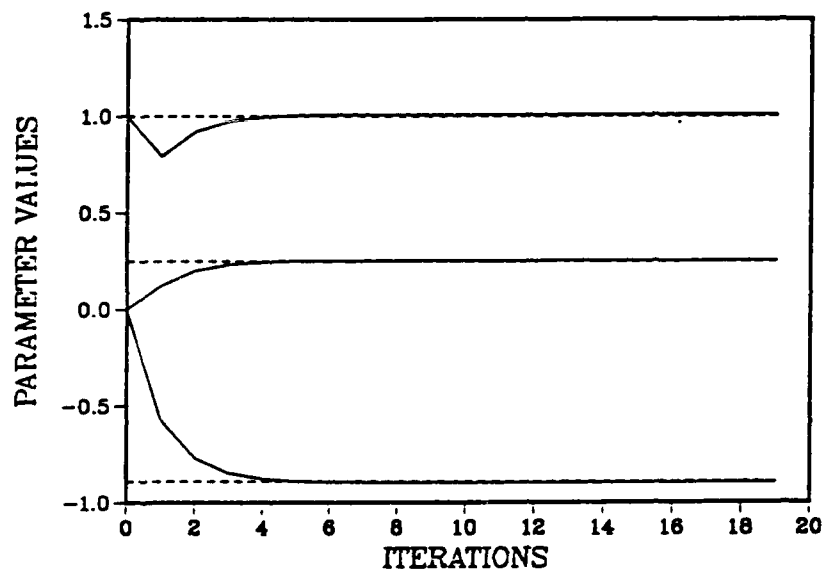
TEST FILTER	LOCATION OF POLES	LOCATION OF ZEROS	AR PARAMETERS	MA PARAMETERS
T2	0.445 + j0.228 0.445 - j0.228	0.4 + j1.273 0.4 - j1.273	1.0 -0.89 0.25	0.5 -0.4 0.89
T2N	0.445 + j0.228 0.445 - j0.228	0.4 + j0.8 0.4 - j0.8	1.0 -0.89 0.25	1.0 -0.80 0.80
T3	0.6605 0.6647 + j0.5020 0.6647 - j0.5020	-1.0 -1.0 -1.0	1.0 -1.99 1.572 -0.4583	0.0154 0.0462 0.0462 0.0154

Results of the tests are shown in graphical form in Figure 8 on page 29, Figure 9 on page 30, and Figure 10 on page 31. Dashed lines indicate the true values of the parameters. Solid lines show the values the algorithm calculated.

Table 4 on page 32 contains the algorithm's best estimates of the parameters, along with the number of iterations required to converge to those estimates. It also shows the absolute and percent errors from the true parameters. For the second-order test cases, convergence to the true parameter values occurred within 20 iterations. The third-order test case took 14 iterations to converge to its steady-state values; however, these values were not the true parameter values.

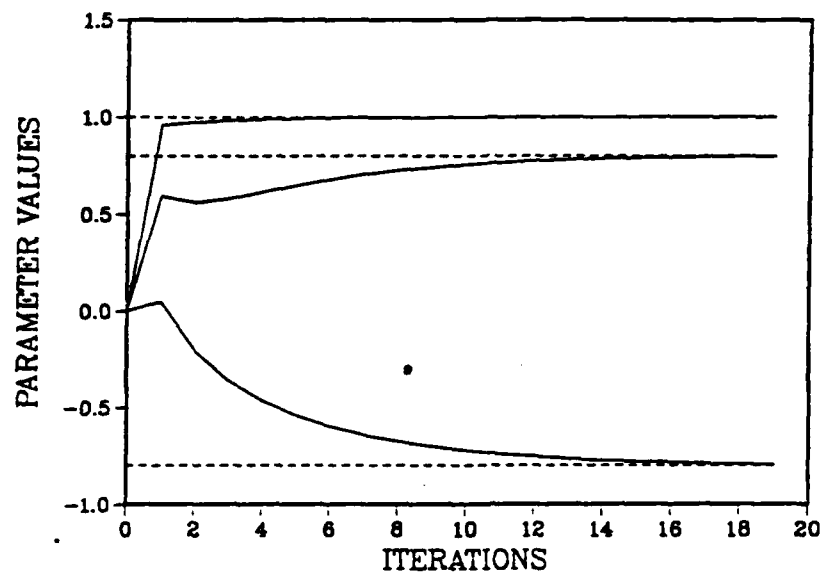


(A)

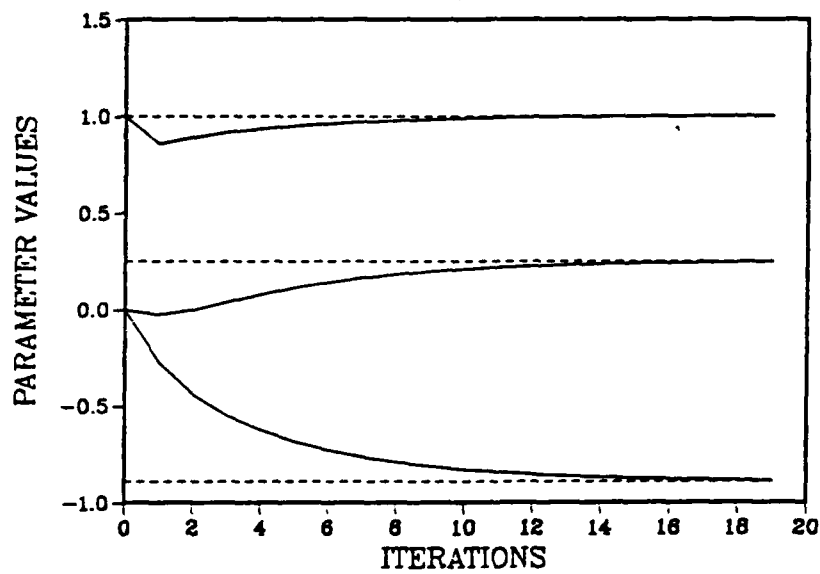


(B)

Figure 8. Second-order test case T2. (A) MA parameters. (B) AR parameters.

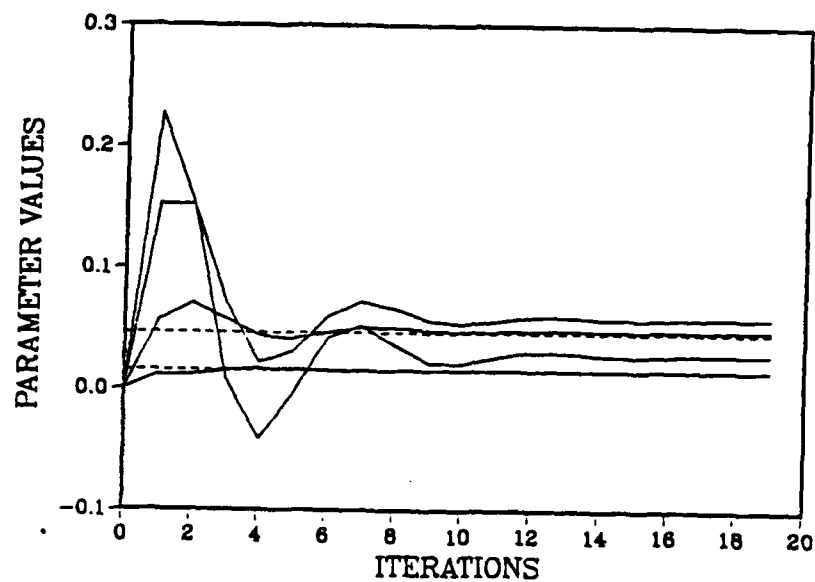


(A)

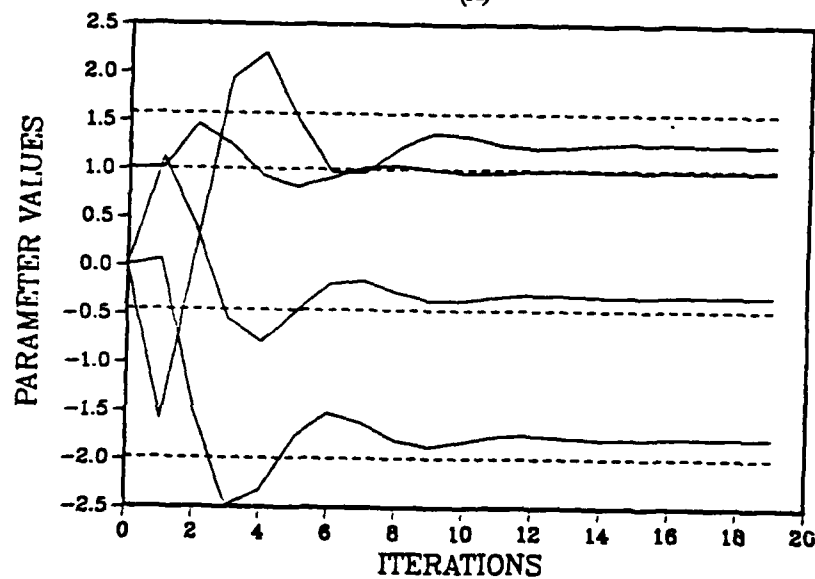


(B)

Figure 9. Second-order test case T2N. (A) MA parameters. (B) AR parameters.



(A)



(B)

Figure 10. Third-order test case T3. (A) MA parameters. (B) AR parameters.

Table 4. PARAMETER ESTIMATES BY THE ITERATIVE MULTICHANNEL ALGORITHM.

TEST FILTER	PARAMETER ESTIMATE	ABSOLUTE ERROR	PERCENT ERROR	ITERATIONS
T2	0.500	0.0	0.0	5
	-0.393	-0.007	1.75	
	0.890	0.0	0.0	
	1.000	0.0	0.0	
	-0.889	+0.001	0.11	
	0.247	-0.003	1.20	
T2N	1.000	0.0	0.0	20
	-0.794	+0.006	0.75	
	0.798	-0.002	0.25	
	1.000	0.0	0.0	
	-0.886	+0.004	0.45	
	0.245	-0.005	2.00	
T3	0.0153	-0.0001	0.65	14
	0.0487	+0.0025	5.41	
	0.0590	+0.0128	27.71	
	0.0287	+0.0133	86.36	
	0.99	-0.01	1.0	
	-1.79	+0.20	10.05	
	1.267	-0.305	19.40	
	-0.3086	+0.1497	32.66	

2. Stopping Parameter

In tests of third-order systems, the parameter estimates swung through or close to the true coefficient values and converged to values somewhat removed from the true values. We developed a stopping parameter to flag the iteration when the estimates were closest to the true values. This occurs when the error is smallest. Referring to Figure 7 on page 25, if $D(z)$ is equal to $A(z)$ and $C(z)$ is equal to $B(z)$, x and z will both equal $A(z)U(z)$. The error will be zero. The farther removed $D(z)$ and $C(z)$ are from $A(z)$ and $B(z)$, respectively, the larger the error becomes.

The stopping parameter is calculated from the difference of the z and x values at every iteration. After the parameter vectors d and c are estimated for a particular iteration, the stopping parameter is calculated from:

$$e_k(n) = z_k(n) - x_k(n) = y_k^T c_k - u_k^T d_k \quad (4.25)$$

where k is the iteration number and \mathbf{d} , \mathbf{u} , \mathbf{c} and \mathbf{y} are defined in equations (4.5) to (4.8). The parameter vectors \mathbf{d} and \mathbf{c} represent the systems $\mathbf{D}(z)$ and $\mathbf{C}(z)$, respectively.

Figure 11 on page 34 and Figure 12 on page 35 graph the stopping parameter (dotted line) along with the estimated and true values of the parameters. They show that when the stopping parameter is smallest, the parameters are closest to their true values. Table 5 shows the improvement in the estimates of the parameters resulting from choosing those values when the stopping parameter is smallest.

Table 5. PARAMETER ESTIMATES WHEN STOPPING PARAMETER IS SMALLEST.

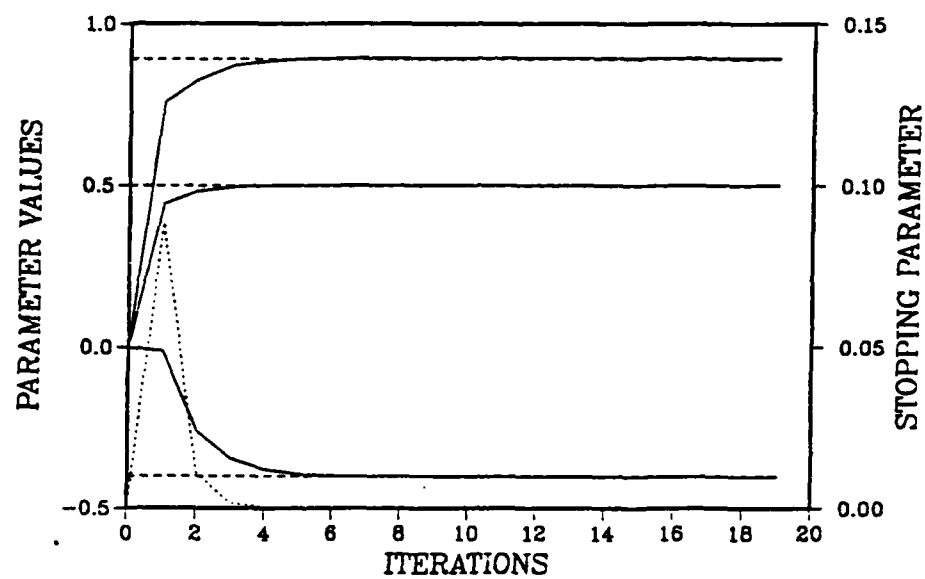
TEST FILTER	PARAMETER ESTIMATE	ABSOLUTE ERROR	PERCENT ERROR	ITERATIONS
T3	0.0156	+ 0.0002	1.30	10
	0.0478	+ 0.0016	3.46	
	0.0536	+ 0.0074	16.02	
	0.0196	+ 0.0042	27.27	
	0.97	-0.03	3.0	
	-1.84	+ 0.15	7.54	
	1.375	-0.197	12.53	
	-0.3672	+ 0.0911	19.88	

The stopping parameter can be used in a real modeling situation because it comes from the data and the estimates of the parameters. Another measure of how well the estimates of the parameters fit the actual system is the norm of the coefficient error. This cannot be used in a real modeling situation however, because the values of the true parameters are not known. We calculated it for the test cases as a check on the appropriateness of using the stopping parameter. Figure 13 on page 36 and Figure 14 on page 37 graph the stopping parameter (dotted line) and the norm of the coefficient error for test cases T2 and T3. On both graphs the two curves correspond well. Both reach their minimum value at the same point, the point where the estimates of the parameters are closest to their true values.

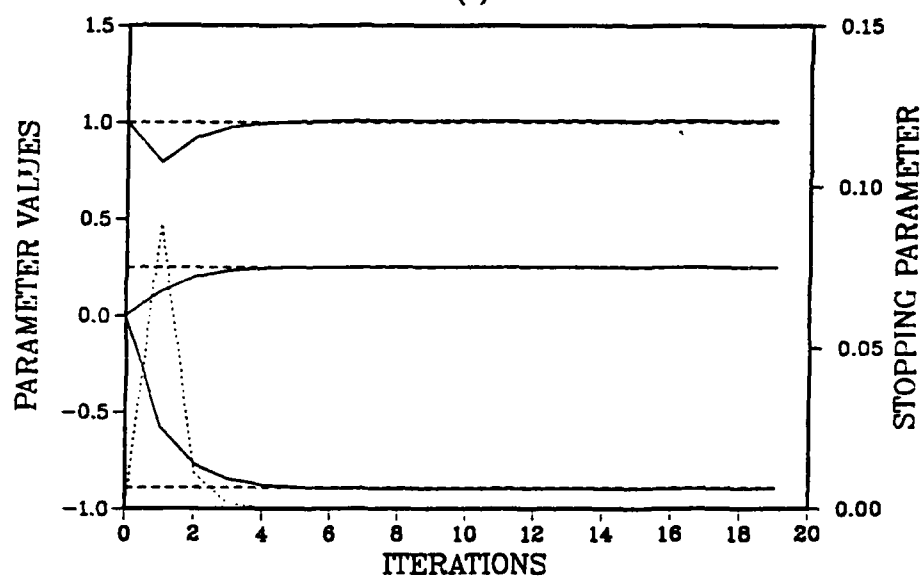
3. Linear-prediction of the Denominator Coefficients

The iterative algorithm detailed in equations (4.22) to (4.24) starts by initializing the AR parameter estimates to:

$$\mathbf{c}^{(0)} = [1 \ 0 \ \dots \ 0]^T \quad (4.26)$$

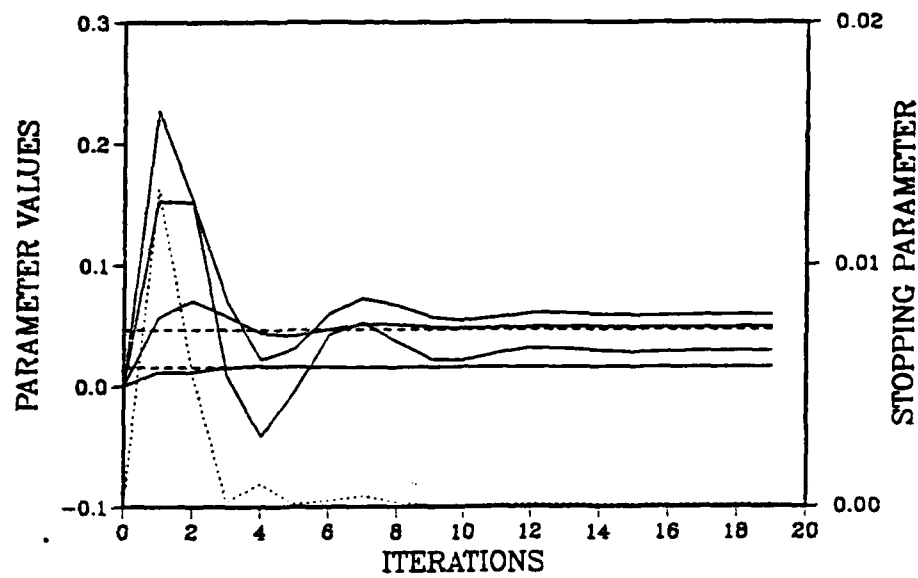


(A)

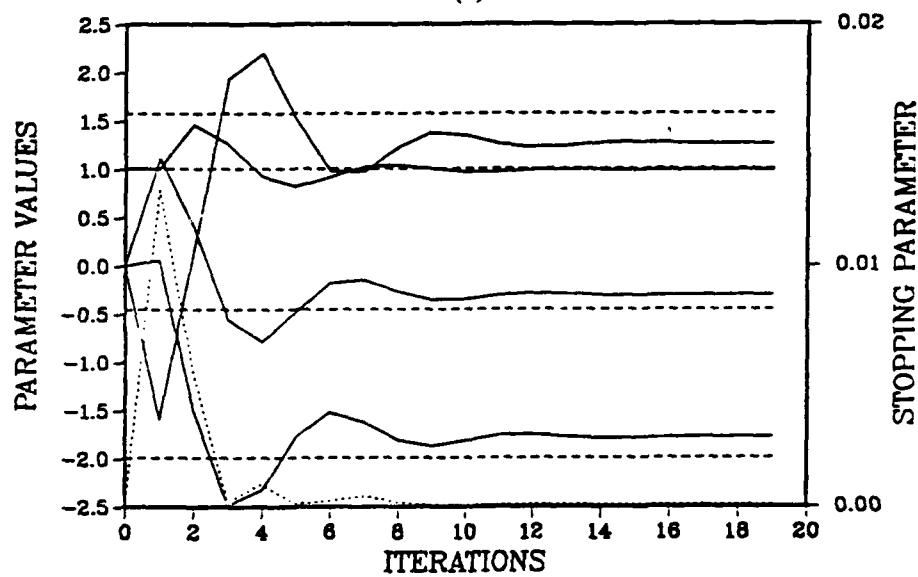


(B)

Figure 11. Stopping parameter example for test case T2.



(A)



(B)

Figure 12. Stopping parameter example for test case T3.

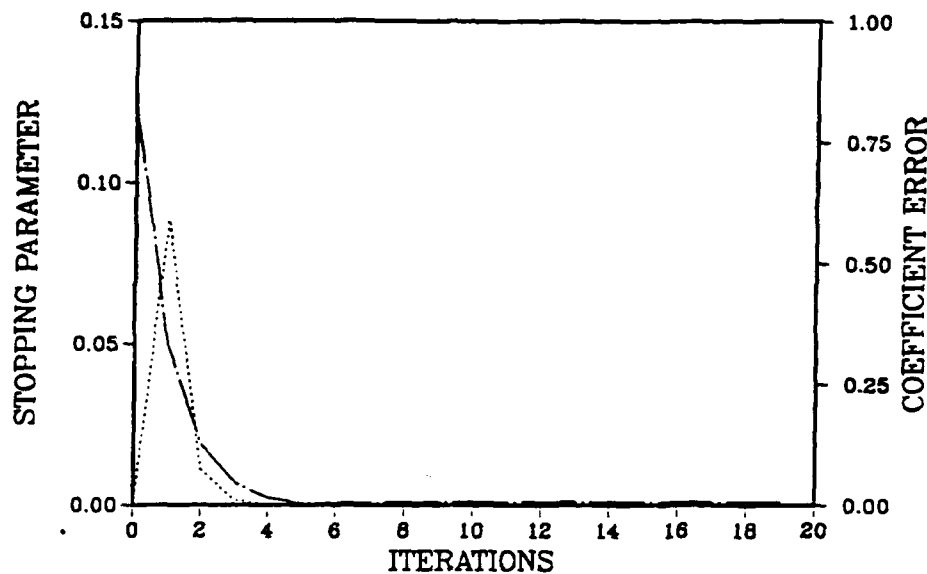


Figure 13. Stopping parameter and norm of the coefficient error for test case T2.

where c_0 is known to be 1 from the Z transform of the ARMA difference equation, equation (2.1). The Z transform is given by:

$$Y(z)[1 + c_1 z^{-1} + c_2 z^{-2} + \dots] = U(z)[d_0 + d_1 z^{-1} + d_2 z^{-2} + \dots] \quad (4.27)$$

$$\frac{Y(z)}{U(z)} = \frac{d_0 + d_1 z^{-1} + d_2 z^{-2} + \dots}{1 + c_1 z^{-1} + c_2 z^{-2} + \dots} \quad (4.28)$$

The initial estimates for the other AR parameters are zero. This can be far from their actual values. A closer estimate of the other AR parameters should result in quicker convergence for all parameters. A closer estimate of the AR parameters can be obtained by using linear-prediction techniques. Figure 15 on page 39 shows the approach used. In Figure 15 on page 39, $y(n)$ is the output from the unknown system. The system $C'(z)$, which is represented by the vector c' , is the linear-prediction filter used to estimate $y(n)$. It uses the previous $n - N$ samples of the output to generate a current estimate. This is given by the equation:

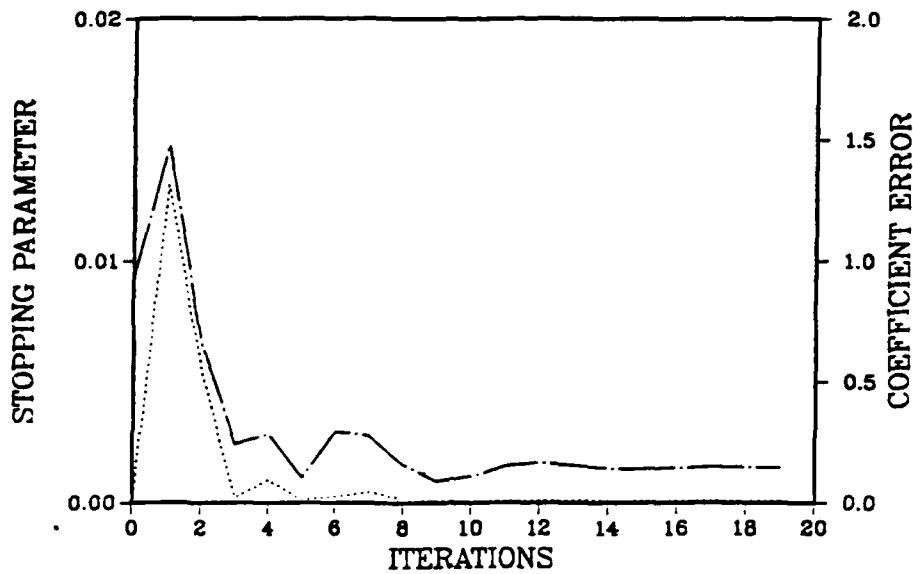


Figure 14. Stopping parameter and norm of the coefficient error for test case T3.

$$\hat{y}(n) = y^T(n-1)c' \quad (4.29)$$

where c' is a vector of the tap weights of the autoregressive process given by:

$$c' = [c'_0 \ c'_1 \ \dots \ c'_{n-N}]^T \quad (4.30)$$

and $y(n-1)$ is a vector of the past output values given by:

$$y(n-1) = [y(n-1) \ y(n-2) \ \dots \ y(n-N)]^T \quad (4.31)$$

Following least-squares techniques, we form the error between the estimate and the actual value of the output. The sum of the squares of the errors becomes the performance criterion. This is differentiated with respect to the tap weights and set equal to zero. Solving this for the tap weights results in the equation:

$$c' = R_{yy}^{-1} r_{yy} \quad (4.32)$$

This is the standard Weiner filter solution [Ref. 8: p. 32]. It tells us that the best estimate of the AR parameters can be found from the correlations of the output data. The matrix R_{yy} is the autocorrelation matrix of the past outputs and r_{yy} is autocorrelation vector of the past outputs with the current output. In all cases tested, we did not achieve any significant improvement in the accuracy of the estimates of the parameters, or in the speed of convergence, using the straight linear prediction of equation (4.32).

A modification to this approach, which we refer to as modified linear-prediction, uses correlation lags beginning on the order of the MA portion of the ARMA process. For example, correlations for calculating R_{yy} for a third-order system would start at a lag of three and increase to a lag of five. Correlations for calculating r_{yy} would start at a lag of four and increase to a lag of six. This ensures that the effect of the MA part of the unknown system is removed from the linear-prediction of the AR part. This modified method of linear-prediction is given by the equation:

$$\begin{bmatrix} c'_0 \\ c'_1 \\ \vdots \\ c'_{n-N} \end{bmatrix} = \begin{bmatrix} r_{yy}(q) & r_{yy}(q-1) & \cdots & r_{yy}(q-p+1) \\ r_{yy}(q+1) & r_{yy}(q) & \cdots & r_{yy}(q-p+2) \\ \vdots & \vdots & \ddots & \vdots \\ r_{yy}(q+p-1) & r_{yy}(q+p-2) & \cdots & r_{yy}(q) \end{bmatrix} \begin{bmatrix} r_{yy}(q+1) \\ r_{yy}(q+2) \\ \vdots \\ r_{yy}(q+p) \end{bmatrix} \quad (4.33)$$

where q is the order of the MA portion and p is the order of the AR portion. [Ref. 2: p. 182]

Figure 16 on page 40 shows the results of using modified linear-prediction with third-order test case T3. When comparing this graph to the estimates obtained without linear-prediction, shown in Figure 12 on page 35, note that the vertical axes have different scales. Table 6 on page 39 lists the values of the estimates at iteration 10 and compares them with the true values via the absolute and percent errors. A comparison of Table 6 on page 39 with Table 5 on page 33, the best estimates without the use of modified linear-prediction, shows that modified linear prediction has significantly increased the accuracy of the AR estimates at the tenth iteration. The accuracy of the MA estimates remains approximately the same. The tenth iteration was chosen as the point to select the parameter values because in both cases this was the iteration where the stopping parameter had the smallest value.

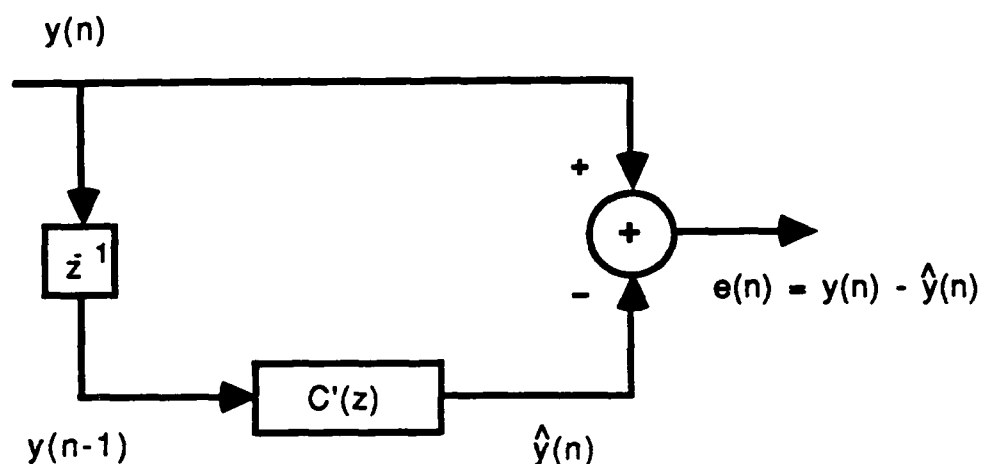


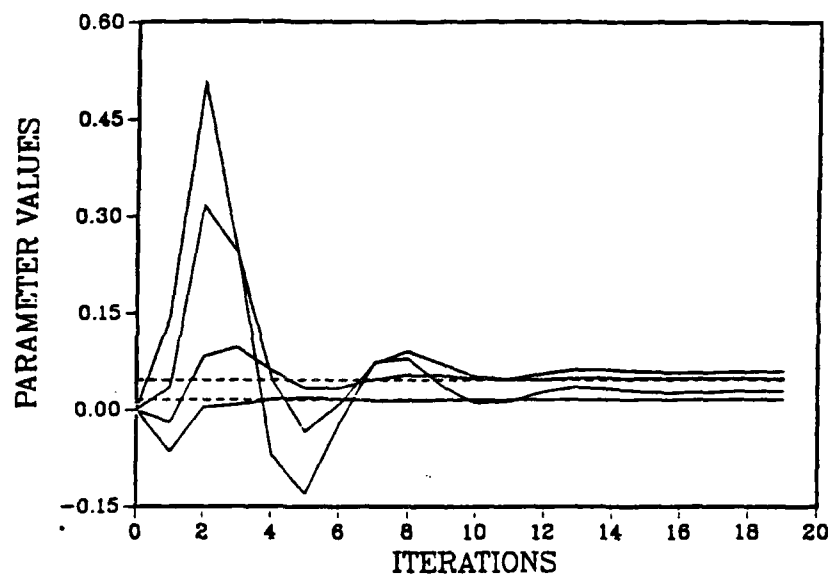
Figure 15. Linear prediction block diagram

Table 6. PARAMETER ESTIMATES USING MODIFIED LINEAR-PREDICTION FOR INITIAL ESTIMATE OF AR PARAMETERS.

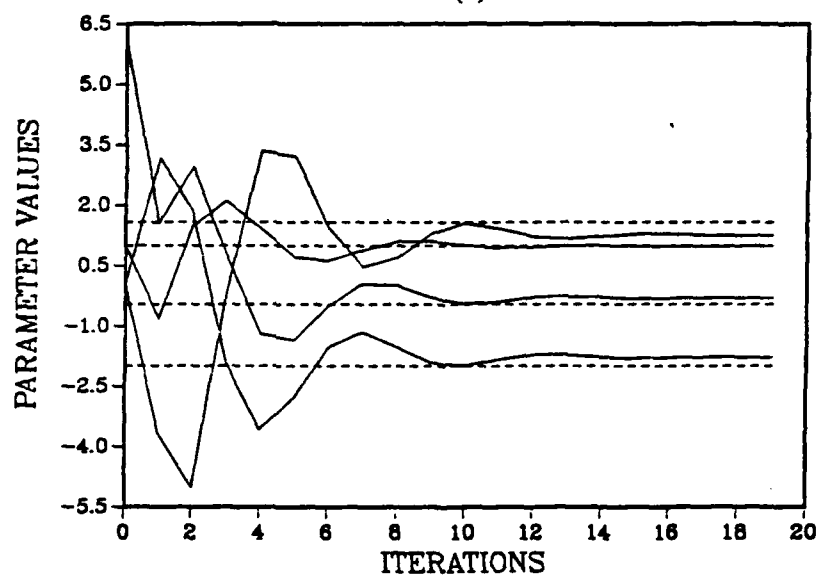
TEST FILTER	PARAMETER ESTIMATE	ABSOLUTE ERROR	PERCENT ERROR	ITERATIONS
T3	0.0156	+0.0002	1.30	10
	0.0485	+0.0023	4.98	
	0.0512	+0.0050	10.80	
	0.0101	+0.0053	34.42	
	1.00	0.0	0.0	
	-1.98	+0.01	0.50	
	1.553	-0.019	1.21	
	-0.4458	+0.0125	2.73	

D. FORMULATION OF THE SEQUENTIAL MULTICHANNEL APPROACH

To decrease the computational intensity of updating the estimates of the AR and MA parameters due to new data, an algorithm to sequentially process the data has been



(A)



(B)

Figure 16. Parameter estimates for test case T3 using modified linear-prediction for initial estimate of AR parameters.

developed. Development begins with the performance criterion seen previously for the block data case in equation (4.10). From that starting point, equations are developed which relate new estimates of the parameters to the previous estimates and the new data. Separate but similar equations are developed for the MA and the AR coefficients. Due to the similar nature of the development of these equations, only the development of the equations for the AR coefficients is presented here. However, the final results for both the AR and MA coefficients are given.

The performance criterion can be written as:

$$J = \sum_{i=0}^n e(i)^2 = \sum_{i=0}^n [z_i - x_i]^2 = \sum_{i=0}^n [z_i - y_i^T c]^2 \quad (4.34)$$

Expanding this results in:

$$J = \sum_{i=0}^n z_i^T z_i - 2z_i^T y_i^T c + c^T y_i y_i^T c \quad (4.35)$$

where c and y are defined in equations (4.7) and (4.8) and z is the scalar signal at the output of D . Differentiating the performance criterion with respect to c and setting the result equal to zero yields:

$$\frac{\partial J}{\partial c} = 0 = \left(\sum_{i=0}^n y_i y_i^T \right) c - \sum_{i=0}^n z_i y_i \quad (4.36)$$

Equation (4.36) can also be written as

$$\sum_{i=0}^n z_i y_i = \left(\sum_{i=0}^n y_i y_i^T \right) c \quad (4.37)$$

Solving for the AR parameter vector results in:

$$c = \left(\sum_{i=0}^n y_i y_i^T \right)^{-1} \sum_{i=0}^n z_i y_i \quad (4.38)$$

Because \mathbf{c} is an estimate based on data available through time n we signify this by introducing the index n on \mathbf{c} to yield:

$$\mathbf{c}_n = \left(\sum_{i=0}^n \mathbf{y}_i \mathbf{y}_i^T \right)^{-1} \sum_{i=0}^n z_i \mathbf{y}_i \quad (4.39)$$

The first step in formulating the sequential algorithm is to develop an update equation for the estimate of the AR parameters. Applying the method presented in Graupe [Ref. 9: p. 124], we first define a new matrix \mathbf{P}_n^{-1} as

$$\mathbf{P}_n^{-1} = \sum_{i=0}^n \mathbf{y}_i \mathbf{y}_i^T \quad (4.40)$$

This is a matrix of the output data of the unknown system. At the previous time $n-1$ this matrix is written as:

$$\mathbf{P}_{n-1}^{-1} = \sum_{i=0}^{n-1} \mathbf{y}_i \mathbf{y}_i^T \quad (4.41)$$

By substituting equation (4.40) into equation (4.39) the estimate of the AR parameters can be rewritten as:

$$\mathbf{c}_n = \mathbf{P}_n^{-1} \sum_{i=0}^n z_i \mathbf{y}_i \quad (4.42)$$

The right side of equation (4.42) needs to be converted into an expression containing the previous estimate of the parameters plus a correction term. It needs the past value of \mathbf{c}_n which is \mathbf{c}_{n-1} . From equation (4.39) we can write:

$$\mathbf{c}_{n-1} = \left(\sum_{i=0}^{n-1} \mathbf{y}_i \mathbf{y}_i^T \right)^{-1} \sum_{i=0}^{n-1} z_i \mathbf{y}_i \quad (4.43)$$

This can be rewritten as:

$$\sum_{i=0}^{n-1} z_i \mathbf{y}_i = \left(\sum_{i=0}^{n-1} \mathbf{y}_i \mathbf{y}_i^T \right) \mathbf{c}_{n-1} \quad (4.44)$$

Premultiplying equation (4.42) by P_n^{-1} and then separating the last term from the summation results in:

$$P_n^{-1}c_n = \sum_{i=0}^{n-1} z_i y_i + z_n y_n \quad (4.45)$$

Substituting for $\sum_{i=0}^{n-1} z_i y_i$ in equation (4.45) from its equivalent expression in equation (4.44) yields:

$$P_n^{-1}c = \left(\sum_{i=0}^{n-1} y_i y_i^T \right) c_{n-1} + z_n y_n \quad (4.46)$$

By adding $y_n y_n^T c_{n-1}$ to the right side of equation (4.46) and grouping it with the summation, the summation will range from $i = 0$ to n . In order not to affect the value on the right side of equation (4.46), $y_n y_n^T c_{n-1}$ must also be subtracted from the right-hand side, which yields:

$$P_{n-1}^{-1}c = \left(\sum_{i=0}^{n-1} y_i y_i^T \right) c_{n-1} + z_n y_n + y_n y_n^T c_{n-1} - y_n y_n^T c_{n-1} \quad (4.47)$$

Combining $y_n y_n^T c_{n-1}$ with the summation as describe above results in:

$$P_{n-1}^{-1}c = \left(\sum_{i=0}^n y_i y_i^T \right) c_{n-1} + z_n y_n - y_n y_n^T c_{n-1} \quad (4.48)$$

Replacing $\sum_{i=1}^n y_i y_i^T$ with its equivalent expression from equation (4.40) yields:

$$P_n^{-1}c_n = P_n^{-1}c_{n-1} + y_n(z_n - y_n^T c_{n-1}) \quad (4.49)$$

Premultiplying by P_n results in the following equation for the update of the estimate of the AR parameters:

$$c_n = c_{n-1} + P_n y_n(z_n - y_n^T c_{n-1}) \quad (4.50)$$

This is the desired result. It relates the estimate of the parameters at time N to the estimate at the previous time, $N - 1$, plus the new output data vector, y_n , and the error at

time N . Error is represented by the $z_n - y_n^T c_{n-1}$ term. The corresponding equation for the MA parameters is:

$$d_n = d_{n-1} + Q_n u_n (x_n - u_n^T d_{n-1}) \quad (4.51)$$

In equation (4.51), Q is a matrix of the input data of the unknown system given by:

$$Q_n^{-1} = \sum_{i=0}^n u_i u_i^T \quad (4.52)$$

Finally, we need a sequential update for P_n and Q_n to complete the sequential algorithm. This is accomplished by using a form of the matrix inversion lemma.

By pulling the last term out of the summation, the definition of P_n^{-1} given in equation (4.40) can be rewritten as:

$$P_n^{-1} = \sum_{i=0}^{n-1} y_i y_i^T + y_n y_n^T \quad (4.53)$$

Substituting for $\sum_{i=0}^{n-1} y_i y_i^T$ its equivalent expression from equation (4.41) results in

$$P_n^{-1} = P_{n-1}^{-1} + y_n y_n^T \quad (4.54)$$

Inverting both sides of the equation results in:

$$P_n = (P_{n-1}^{-1} + y_n y_n^T)^{-1} \quad (4.55)$$

Let $A = P_{n-1}^{-1}$, $B = y_n$, $C = 1$, and $D = y_n^T$. Then, by the matrix inversion lemma:

$$P_n = A^{-1} - A^{-1} B (C^{-1} + D A^{-1} B)^{-1} D A^{-1} \quad (4.56)$$

Substituting the appropriate expressions into equation (4.56) results in:

$$P_n = (P_{n-1}^{-1})^{-1} - (P_{n-1}^{-1})^{-1} y_n [1 + y_n^T (P_{n-1}^{-1})^{-1} y_n]^{-1} y_n^T (P_{n-1}^{-1})^{-1} \quad (4.57)$$

This reduces to:

$$P_n = P_{n-1} - P_{n-1} y_n [1 + y_n^T P_{n-1} y_n]^{-1} y_n^T P_{n-1} \quad (4.58)$$

Using this same procedure, the update for Q_n is:

$$\mathbf{Q}_n = \mathbf{Q}_{n-1} - \mathbf{Q}_{n-1} \mathbf{u}_n [1 + \mathbf{u}_n^T \mathbf{Q}_{n-1} \mathbf{u}_n]^{-1} \mathbf{u}_n^T \mathbf{Q}_{n-1} \quad (4.59)$$

A reduction in the computational intensity has been achieved by reducing the matrix inversion of equation (4.55) to inversion of a scalar in equation (4.57). Inversion of these scalars is much simpler than inversion of the \mathbf{R}_{yy} and \mathbf{R}_{uu} matrices of the block processing case.

The sequential multichannel algorithm is summarized below:

- The parameter update equations:

$$\mathbf{c}_n = \mathbf{c}_{n-1} + \mathbf{P}_n \mathbf{y}_n (z_n - \mathbf{y}_n^T \mathbf{c}_{n-1}) \quad (4.60)$$

$$\mathbf{d}_n = \mathbf{d}_{n-1} + \mathbf{Q}_n \mathbf{u}_n (x_n - \mathbf{u}_n^T \mathbf{d}_{n-1}) \quad (4.61)$$

- The update equations for the \mathbf{P} and \mathbf{Q} matrices:

$$\mathbf{P}_n = \mathbf{P}_{n-1} - \mathbf{P}_{n-1} \mathbf{y}_n [1 + \mathbf{y}_n^T \mathbf{P}_{n-1} \mathbf{y}_n]^{-1} \mathbf{y}_n^T \mathbf{P}_{n-1} \quad (4.62)$$

$$\mathbf{Q}_n = \mathbf{Q}_{n-1} - \mathbf{Q}_{n-1} \mathbf{u}_n [1 + \mathbf{u}_n^T \mathbf{Q}_{n-1} \mathbf{u}_n]^{-1} \mathbf{u}_n^T \mathbf{Q}_{n-1} \quad (4.63)$$

The reduction in computational intensity comes with a trade-off. Now the algorithm is more complex to use. Updates are required for \mathbf{P} and \mathbf{Q} as well as \mathbf{c} and \mathbf{d} where before, in the block multichannel algorithm, updates were only required for \mathbf{c} and \mathbf{d} . But, as in the sequential IV case, an added advantage of the sequential multichannel algorithm is it allows updates of the estimates of the parameters based upon new data.

V. SUMMARY

In this thesis we set out to develop two algorithms for modeling unknown systems as ARMA processes. These are the IV method of system identification presented in Chapter 3, which is a modification of the method of ordinary least-squares, and the iterative multichannel method presented in Chapter 4.

The IV method is not a new concept in either its block or sequential processing forms. However, our derivation of the sequential algorithm was done independently of other IV sequential algorithms. We chose the IV method because it reportedly has good noise handling capabilities and yields consistent and unbiased estimates of the unknown system's parameters. It also remains as easy to use as the method of ordinary least-squares. We also wanted to gain familiarity with it because it was a possible candidate for incorporation into the multichannel method.

Operating alone, the IV method produces accurate estimates of the unknown system's parameters. Convergence was within 20 iterations for several second-order systems that we tested. Convergence slows down as the system order increases. However, the results do converge to the actual system parameters given sufficient processing time. The performance of the IV method is similar to the performance of the method of ordinary least-squares.

The proposed iterative multichannel algorithm is new in both its block and sequential processing forms to the best of our knowledge. It is very simple to use in the block form. It achieves accurate results for second-order systems but worse results for third-order systems with block correlation elements calculated based on only 500 data points. Implementing the stopping parameter increases the accuracy when the parameter estimates converge but not to the true parameters. Due to its ability to separately process the input and output data from the unknown system, correlation matrices in the multichannel block processing case are half the size of correlation matrices required for the single channel block processing case. This feature reduces the computational intensity over what is required for the conventional least-squares processing case. The number of iterations required for convergence seems to be independent of the order of the system. However, the accuracy of the estimates suffer as the order of the system increases. Using linear prediction to estimate the initial values of the AR parameters did not speed up convergence or increase the accuracy of the parameter estimates. However, using

modified linear prediction significantly increased the accuracy of the AR parameter estimates, although it had no effect on the MA parameter estimates.

We formulated the multichannel sequential algorithm. This allows the estimates of the parameters to be updated as new data becomes available. But we have not tested this algorithm. It needs checking using a variety of second and third-order test cases to verify that it works. During testing, guidelines need to be developed for the best methods to initialize the P and Q matrices to achieve the quickest convergence and the most accurate parameter estimates.

As mentioned above, one of the reasons for investigating the IV method of system identification was for possible inclusion into the multichannel algorithm, the hope being that the favorable noise performance of the IV method would improve the performance of the multichannel method. This is another area that remains unexplored.

The block multichannel and IV methods achieved similar results for second-order test cases. Convergence to the actual system parameters came within 20 iterations for both algorithms. However, for third-order systems, convergence was much quicker with the multichannel block algorithm than with the sequential IV algorithm. But the parameter estimates by the IV method were more accurate than by the multichannel block method. A combination of the two algorithms has the potential for incorporating their unique advantages into a better overall parameter estimation method.

Areas for further research are listed below:

- Verify that the multichannel sequential algorithm developed in Chapter 4 works as a means of modeling an unknown system as an ARMA process.
- Investigate the possibility of incorporating the IV method into the multichannel sequential algorithm.
- Analyze why initializing the AR parameters to the values calculated by linear prediction improves the speed of convergence of the AR parameters in the multichannel block algorithm but does not improve the convergence of the MA parameters. Identify a method for obtaining an initial estimate of the MA parameters to improve their speed of convergence and accuracy.
- Investigate the effects of increasing the number of data points used to calculate the correlation matrices for the multichannel block algorithm on the accuracy of the parameter estimates and their speed of convergence.
- Investigate the performance of the IV method with noise present. Compare this performance with the performance of the method of ordinary least-squares with noise present.

APPENDIX

A. INSTRUMENTAL VARIABLE ALGORITHM

```

*****
*
*          PAUL DAL SANTO
*          IV ALGORITHM
*          4/12/88
*
* THIS PROGRAM CALCULATES THE AR AND MA PARAMETERS OF A
* TEST SYSTEM BASED UPON ITS INPUT AND OUTPUT DATA
* BY USING THE SEQUENTIAL IV METHOD.
*
*****
I
V
A
0
0
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1
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I
V
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I
V
A
0
0
0
3
0
I
V
A
0
0
0
4
0
I
V
A
0
0
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5
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I
V
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**** VARIABLE DEFINITIONS ****

* RIVCOF  ARRAY FOR STORING THE AR AND MA PARAMETERS
*          THE PROGRAM CALCULATES
* Z        VECTOR OF DATA FROM THE OUTPUT OF THE AUXILIARY
*          MODEL AND THE INPUT TO THE TEST SYSTEM
* Z TPO    TRANSPOSE OF VECTOR Z
* X        VECTOR OF DATA FROM THE OUTPUT AND INPUT OF THE
*          TEST SYSTEM
* X TPO    TRANSPOSE OF THE X VECTOR
* U        STORAGE FOR INPUT DATA
* Y        STORAGE FOR OUTPUT OF TEST SYSTEM
* W        STORAGE FOR OUTPUT OF THE AUXILIARY MODEL
* QMAT     THE Q MATRIX OF THE IV ALGORITHM
* IV       VECTOR OF PARAMETERS CALCULATED BY THE ALGORITHM
* COR      RESULT OF INTERMEDIATE STEP IN ALGORITHM CALCULATION
* COEF     VECTOR OF TRUE PARAMETERS OF TEST SYSTEM
* SCALAR   RESULT OF SCALAR INVERSION IN INTERMEDIATE STEP COR
* SCALR2   INTERMEDIATE STEP WHEN CALCULATING THE NEW IV VECTOR
* SEED     INITIALIZATION FOR IMSL GAUSSIAN ROUTINE
* WSIZE    ORDER OF AR PART OF THE AUXILIARY MODEL
* YSIZE    ORDER OF THE AR PART OF THE TEST SYSTEM
* USIZE    ORDER OF THE MA PART OF THE TEST SYSTEM AND AUXILIARY
*          MODEL

* VARIABLES THAT END IN R CONTAIN THE ROW SIZE OF THEIR RESPECTIVE
* MATRICES. VARIABLES THAT END IN C CONTAIN THE COLUMN SIZE OF
* THEIR RESPECTIVE MATRICES.

**** VARIABLE DECLARATIONS ****

COMMON /D/ RIVCOF(0:1000,10)

REAL Z(10,10),Z TPO(10,10),X(10,10),X TPO(10,10)
REAL U(1),Y(10,10),W(10,10)

```


REAL QMAT(10,10),Q TEMP(10,10),QTEMP2(10,10),QTEMP3(10,10)	IVA00490
REAL IV(10,10),IVTEMP(10,10),COR(10,10),COEF(10,10)	IVA00500
REAL SCALAR,SCALR2	IVA00510
	IVA00520
DOUBLE PRECISION SEED	IVA00530
	IVA00540
INTEGER I,J,K,WSIZE,YSIZE,USIZE	IVA00550
INTEGER ZMR,ZMC,ZTR,ZTC,XMR,XMC,XTR,UTC	IVA00560
INTEGER UMR,UMC,YMR,PMC,WMR,PMC	IVA00570
INTEGER QMR,QMC,QTR,UTC,QT2R,QT2C,QT3R,QT3C	IVA00580
INTEGER IVR,IVC,IVTR,IVTC,CMR,PMC,COEFMR,COEFMC	IVA00590
INTEGER IVCR,IVCC	IVA00600
LOGICAL EOF	IVA00610
	IVA00670
READ(4,*,END=22) YSIZE,USIZE,COEFMR,COEFMC,ITERA	IVA00680
CALL RDMAT(COEF,COEFMR,COEFMC)	IVA00690
* INITIALIZE VARIABLES	IVA00700
	IVA00630
EOF = .FALSE.	IVA00640
XTR = COEFMC	IVA00650
UTC = COEFMR	IVA00710
ZTR = COEFMC	IVA00720
ZTC = COEFMR	IVA00730
IVR = COEFMR	IVA00740
IVC = COEFMC	IVA00750
QMR = COEFMR	IVA00760
QMC = COEFMR	IVA00770
SEED = 888.0D1	IVA00780
IVCR = 0	IVA00790
IVCC = COEFMR	IVA00800
WSIZE = YSIZE	IVA00810
	IVA00820
	IVA00830
* ZERO OUT THE IV PARAMETER VECTOR, THE AUXILIARY MODEL DATA VECTOR	IVA00840
* AND THE TEST SYSTEM DATA VECTOR.	IVA00850
	IVA00860
CALL INIT(IV,IVR,IVC,0.0)	IVA00870
CALL INIT(Z TPO,ZTR,ZTC,0.0)	IVA00880
CALL INIT(X TPO,XTR,UTC,0.0)	IVA00890
	IVA00900
* INITIALIZE THE QMAT AS A DIAGONAL MATRIX WHOSE DIAGONAL ELEMENTS	IVA00910
* EQUAL 100	IVA00920
	IVA00930
CALL INITD(QMAT,QMR,QMC,100.0)	IVA00940
	IVA00950
* GET VALUE FOR U(0). U IS A GAUSSIAN RANDOM VARIABLE.	IVA00960
	IVA00970
CALL GGNML (SEED,1,U)	IVA00990
	IVA01000
* SHIFT U(0) INTO X & Z VECTORS TO CREATE X(0) & Z(0)	IVA01010
	IVA01020
Y(1,1) = 0.0	IVA01030
CALL SHIFT(X TPO,UTC,YSIZE,USIZE,Y(1,1),U(1))	IVA01040
W(1,1) = 0.0	IVA01050
CALL SHIFT(Z TPO,ZTC,WSIZE,USIZE,W(1,1),U(1))	IVA01060

* CALCULATE $Y(0) = X \text{ TPO}(0) * \text{COEFFICIENT VECTOR}$	IVA01070
CALL MULTI(X TPO,XTR,XTC,COEF,COEFMR,COEFMC,Y,1,1)	IVA01080
* CALCULATE $W(0) = Z \text{ TPO}(0) * \text{IV VECTOR}$	IVA01090
CALL MULTI(Z TPO,ZTR,ZTC,IV,IVR,IVC,W,1,1)	IVA01100
DO 90 I = 0,ITERA	IVA01110
CALL GGNML(SEED,1,U)	IVA01120
CALL TPOSE(IV,IVR,IVC,IVTEMP,IVTR,IVTC)	IVA01130
* SAVE THE IV PARAMETERS	IVA01140
DO 91 J = 1,IVTC	IVA01160
RIVCOF(I,J) = IVTEMP(1,J)	IVA01180
91 CONTINUE	IVA01200
CALL PRMAT(IVTEMP,IVTR,IVTC)	IVA01210
* SHIFT $Y(M)$ AND $U(M+1)$ INTO $X \text{ TPO}(M)$ TO GET $X \text{ TPO}(M+1)$	IVA01220
CALL SHIFT(X TPO,XTC,YSIZE,USIZE,Y(1,1),U(1))	IVA01230
* SHIFT $W(M)$ AND $U(M+1)$ INTO $Z \text{ TPO}(M)$ TO GET $Z \text{ TPO}(M+1)$	IVA01240
CALL SHIFT(Z TPO,ZTC,WSIZE,USIZE,W(1,1),U(1))	IVA01250
* CALCULATE $Y(M+1)$ AND $Z(M+1)$	IVA01260
CALL MULTI(X TPO,XTR,XTC,COEF,COEFMR,COEFMC,Y,1,1)	IVA01280
CALL MULTI(Z TPO,ZTR,ZTC,IV,IVR,IVC,W,1,1)	IVA01290
* CALCULATE THE NEW Q MATRIX	IVA01300
CALL MULTI(X TPO,XTR,XTC,QMAT,QMR,QMC,Q TEMP,QTR,QTC)	IVA01320
CALL TPOSE(Z TPO,ZTR,ZTC,Z,ZMR,ZMC)	IVA01330
CALL CORE(CMAT,QMR,QMC,Z,ZMR,ZMC,X TPO,XTR,XTC,COR,CMR,CMC)	IVA01340
CALL MULTI(COR,CMR,CMC,Q TEMP,QTR,QTC,QTEMP2,QT2R,QT2C)	IVA01360
CALL SUBTRC(QMAT,QMR,QMC,QTEMP2,QT2R,QT2C,QMAT,QMR,QMC)	IVA01370
* CALCULATE THE NEW IV VECTOR	IVA01380
CALL MULTI(X TPO,XTR,XTC,IV,IVR,IVC,IVTEMP,IVTR,IVTC)	IVA01400
SCALR2 = $Y(1,1) - \text{IVTEMP}(1,1)$	IVA01410
CALL SMULTI(SCALR2,COR,CMR,CMC)	IVA01420
CALL ADD(IV,IVR,IVC,COR,CMR,CMC,IV,IVR,IVC)	IVA01430
90 CONTINUE	IVA01440
* PLOT THE IV PARAMETERS VS THE ITERATION NUMBER	IVA01450
CALL PLOT2(ITERA,USIZE,YSIZE,COEF)	IVA01460
22 STOP	IVA01470
END	IVA01480
* *****	IVA01490
SUBROUTINE CORE(MAT1,I1R,I1C,MAT2,I2R,I2C,MAT3,I3R,I3C,RMAT,IRR,	IVA01500
+IRC)	IVA01510
* *****	IVA01520
	IVA01530
	IVA01540
	IVA01550
	IVA01560
	IVA01570
	IVA01590
	IVA01600
	IVA01610
	IVA01630
	IVA01640
	IVA01650
	IVA01660
	IVA01670
	IVA01930
	IVA01940
	IVA01950
	IVA01960

REAL MAT1(10,10),MAT2(10,10),MAT3(10,10),RMAT(10,10)	IVA01970
REAL Q TEMP(10,10),QTEMP2(10,10)	IVA02000
INTEGER IRR,IRC,QTR,QTC,QT2R,QT2C	IVA02010
* CALCULATE THE CORE: $Q(M)Z(M+1)^0 1+X'(M+1)Q(M)Z(M+1) ** -1$	IVA02020
* MAT1 IS THE Q MATRIX, MAT2 IS THE Z VECTOR, AND MAT3 IS THE	IVA02030
* X VECTOR.	IVA02040
CALL MULTI(MAT1,I1R,I1C,MAT2,I2R,I2C,Q TEMP,QTR,QTC)	IVA02060
CALL MULTI(MAT3,I3R,I3C,Q TEMP,QTR,QTC,QTEMP2,QT2R,QT2C)	IVA02070
SCALAR = 1/(1 + QTEMP2(1,1))	IVA02090
CALL SMULTI(SCALAR,Q TEMP,QTR,QTC)	IVA02100
CALL ADD(Q TEMP,QTR,QTC,Q TEMP,QTR,QTC,RMAT,IRR,IRC)	IVA02110
CALL SMULTI(0.5,RMAT,IRR,IRC)	IVA02120
RETURN	IVA02130
END	IVA02140
* *****	IVA02150
SUBROUTINE PLOT2(ITERA,ICURVN,ICURVD,MAT1)	IVA02170
* *****	IVA02180
COMMON /D/ RIVCOF(0:1000,10)	IVA02190
REAL X(0:1000),Y(0:1000),MAT1(10,10),MAX,MIN	IVA03720
INTEGER I,J,ITERA,ICURVN,ICURVD,ISTP	IVA03730
CALL LIMITS(ICURVN,ICURVD,NMAX,NMIN,NSTP,	IVA03740
+DMAX,DMIN,DSTP,ITERA)	IVA03750
* GENERATE THE ITERATION NUMBER	IVA03760
DO 90 I = 0,ITERA	IVA03780
X(I) = I	IVA03800
Y(I) = 0.0	IVA03810
90 CONTINUE	IVA03820
* CALCULATE X AXIS LABELING INTERVAL	IVA03830
ISTP = ITERA/10	IVA03850
* SET UP THE PLOT	IVA03860
CALL SHERPA('IVGRAF ','A',3)	IVA03870
CALL RESET('ALL')	IVA03880
CALL PAGE(8.5,11.0)	IVA03890
CALL HEIGHT(0.14)	IVA03900
CALL HWROT('AUTO')	IVA03910
CALL XINTAX	IVA03920
CALL YAXANG(0)	IVA03930
CALL PHYSOR(1.5,6.0)	IVA03950
CALL AREA2D(5.0,3.5)	IVA03960
CALL COMPLX	IVA03970
CALL XNAME('ITERATIONSS',100)	IVA03980
CALL YNAME('COEFFICIENT VALUES',100)	IVA04010
CALL MESSAG('(A)\$',100,2.4,-0.8)	IVA04030
CALL THKFRM(0.03)	IVA04040
CALL FRAME	IVA04050
	IVA04060
	IVA04070
	IVA04080
	IVA04090
	IVA04100
	IVA04110
	IVA04140
	IVA04150
	IVA04160
	IVA04170
	IVA04180

CALL GRAF(0,ISTP,ITERA,NMIN,NSTP,NMAX)	IVA04190
* PLOT THE NUMERATOR VALUES	IVA04210
DO 93 J = ICURVD + 1,ICURVN + ICURVD	IVA04230
DO 94 I = 0,ITERA	IVA04240
Y(I) = RIVCOF(I,J)	IVA04260
94 CONTINUE	IVA04270
CALL CURVE(X,Y,ITERA,0)	IVA04280
93 CONTINUE	IVA04290
* PLOT DASHED LINES FOR THE COEFS' TRUE VALUES	IVA04300
CALL DASH	IVA04310
* PLOT NUMERATOR COEFS' TRUE VALUES	IVA04320
DO 95 K = ICURVD + 1,ICURVD + ICURVN	IVA04330
DO 96 J = 0,ITERA	IVA04350
Y(J) = MAT1(K,1)	IVA04360
96 CONTINUE	IVA04370
CALL CURVE(X,Y,ITERA,0)	IVA04380
95 CONTINUE	IVA04390
CALL ENDGR(0)	IVA04400
* SET UP SECOND PLOT FOR DENOMINATOR PARAMETERS	IVA04410
CALL RESET('DASH')	IVA04420
CALL PHYSOR(1.5,1.5)	IVA04430
CALL AREA2D(5.0,3.5)	IVA04440
CALL COMPLX	IVA04450
CALL XNAME('ITERATIONSS',100)	IVA04460
CALL YNAME('PARAMETER VALUES',100)	IVA04470
CALL MESSAG('(B)\$',100,2.4,-0.8)	IVA04480
CALL THKFRM(0.03)	IVA04490
CALL FRAME	IVA04500
CALL GRAF(0,ISTP,ITERA,DMIN,DSTP,DMAX)	IVA04510
* PLOT THE DENOMINATOR VALUES	IVA04520
DO 91 J = 1,ICURVD	IVA04550
DO 92 I = 0,ITERA	IVA04560
Y(I) = -RIVCOF(I,J)	IVA04570
92 CONTINUE	IVA04580
CALL CURVE(X,Y,ITERA,0)	IVA04590
91 CONTINUE	IVA04600
* PLOT DENOMINATOR COEFS' TRUE VALUES	IVA04610
CALL DASH	IVA04620
DO 99 K = 1,ICURVD	IVA04630
DO 100 J = 0,ITERA	IVA04640
Y(J) = -MAT1(K,1)	IVA04650
100 CONTINUE	IVA04660
CALL CURVE(X,Y,ITERA,0)	IVA04670
99 CONTINUE	IVA04680
	IVA04690
	IVA04700
	IVA04710
	IVA04720
	IVA04730
	IVA04740
	IVA04750
	IVA04760
	IVA04770
	IVA04780
	IVA04790
	IVA04800

CALL ENDPL(0)	IVA04810
CALL DONEPL	IVA04820
RETURN	IVA04830
END	IVA04840
* *****	IVA04850
* SUBROUTINE SUBTRC(MAT1,I1R,I1C,MAT2,I2R,I2C,RMAT,IRR,IRC)	IVA05760
* *****	IVA05770
	IVA05780
**** PURPOSE - ROUTINE SUBTRACTS MAT2 FROM MAT1 AND PUTS THE	IVA05790
* RESULT IN A THIRD MATRIX.	IVA05800
	IVA05810
	IVA05820
REAL MAT1(10,10),MAT2(10,10),RMAT(10,10)	IVA05850
INTEGER IRR,IRC	IVA05860
	IVA05870
CALL SMULTI(-1.0,MAT2,I2R,I2C)	IVA05880
CALL ADD(MAT1,I1R,I1C,MAT2,I2R,I2C,RMAT,IRR,IRC)	IVA05890
IRR = I1R	IVA05900
IRC = I1C	IVA05910
RETURN	IVA05920
END	IVA05930
	IVA05940
* *****	IVA05970
* SUBROUTINE TPOSE(MAT1,I1R,I1C,RMAT,IRR,IRC)	IVA05980
* *****	IVA05990
	IVA06000
**** PURPOSE-SUBROUTINE TRANSPOSES A MATRIX AND PUTS THE RESULT	IVA06010
INTO A NEW MATRIX	IVA06020
	IVA06030
REAL MAT1(10,10),RMAT(10,10)	IVA06040
INTEGER I,J,IRR,IRC	IVA06050
	IVA06060
DO 93 I=1,I1C	IVA06070
DO 94 J=1,I1R	IVA06080
RMAT(I,J) = MAT1(J,I)	IVA06090
94 CONTINUE	IVA06100
93 CONTINUE	IVA06110
IRR = I1C	IVA06120
IRC = I1R	IVA06130
RETURN	IVA06140
END	IVA06150

B. MULTICHANNEL ALGORITHM

C *****	DUA00010
C *	DUA00020
C * PAUL DAL SANTO 8/15/88	DUA00030
C *	DUA00040
C * TWO-CHANNEL SYSTEM IDENTIFICATION ALGORITHM	DUA00050
* *	DUA00060
* *	DUA00070
* *	DUA00080
* *	DUA00090
* *	DUA00100
C *	DUA00110
C * SHIFT USED TO CALC RYY FOR THE LINEAR	

C	*	OF THE AR PARAMETERS IS READ FROM	*	DUA00120
*	*	THE COEFF DATA FILE	*	DUA00130
C	*		*	DUA00140
C	*	NUMBER OF ITERATIONS IS READ FROM COEFF	*	DUA00150
C	*	DATA FILE	*	DUA00160
C	*		*	DUA00170
C	*		*	DUA00180
C	*		*	DUA00190
C	*	*****	*	DUA00200
				DUA00210
*	****	VARIABLE DEFINITIONS	****	DUA00220
				DUA00230
*	RAWDAT	ARRAY WHICH CONTAINS THE INPUT AND OUTPUT DATA		DUA00240
*		OF THE SYSTEM UNDER TEST		DUA00250
*	E1	ARRAY FOR STORING THE STOPPING PARAMETER AND THE		DUA00260
*		COEFFICIENT ERROR		DUA00270
*	ARRD	ARRAY FOR STORING THE AR PARAMETER ESTIMATES		DUA00280
*	ARRN	ARRAY FOR STORING THE MA PARAMETER ESTIMATES		DUA00290
*	RYYM	AUTOCORRELATION MATRIX OF THE OUTPUT DATA		DUA00300
*	RYUM,RUYM	CROSSCORRELATION MATRICES		DUA00310
*	RUUM	AUTOCORRELATION MATRIX OR THE INPUT DATA		DUA00320
*	RUUINV	INVERSE OF THE AUTOCORRELATION MATRIX OF THE INPUT DATA		DUA00330
*	RYYINV	INVERSE OF THE AUTOCORRELATION MATRIX OF THE OUTPT DATA		DUA00340
*	DM	VECTOR OF CURRENT MA PARAMETER ESTIMATES		DUA00350
*	CM	VECTOR OF CURRENT AR PARAMETER ESTIMATES		DUA00360
*	TRUNRM	FUNCTION WHICH CALCULATES THE NORM OF THE TRUE VALUES		DUA00370
*		OF THE TEST SYSTEM'S PARAMETERS		DUA00380
*	WKMAT	WORKING MATRIX FOR DOING MATRIX INVERSIONS		DUA00390
*	X TPO	TRANSPOSE OF THE VECTOR OF INPUT DATA		DUA00400
*	Y	MATRIX FOR THE OUTPUT OF THE TEST SYSTEM		DUA00410
*	U	INPUT TO THE TEST SYSTEM		DUA00420
*	COEFM	VECTOR OF TRUE COEFFICIENTS OF THE TEST SYSTEM		DUA00430
*	ITERA	NUMBER OF ITERATIONS TO PERFORM		DUA00440
*	CORRLN	LENGTH OF CORRELATIONS TO USE TO CALCULATE RYY, RUU		DUA00450
*		RYU, AND RUY		DUA00460
*	ysize	ORDER OF THE AR PART OF THE TEST SYSTEM		DUA00470
*	usize	ORDER OF THE MA PART OF THE TEST SYSTEM		DUA00480
*	KTIME	THE CURRENT ITERATION		DUA00490
*	SHFT	SIZE OF THE STARTING LAG FOR LINEAR PREDICTION OF		DUA00500
*		THE AR PARAMETERS		DUA00510
*	SEED	INITIALIZATION PARAMETER FOR IMSL ROUTINE WHICH		DUA00520
*		GENERATES RANDOM GAUSSIAN NUMBERS		DUA00530
				DUA00540
*		INTEGER VARIABLES THAT END WITH R CONTAIN THE ROW SIZE OF		DUA00550
*		A PARTICULAR ARRAY. INTEGER VARIABLES THAT END WITH C CONTAIN		DUA00560
*		THE COLUMN SIZE OF A PARTICULAR ARRAY.		DUA00570
				DUA00580
*	****	VARIABLE DECLARATIONS	****	DUA00590
				DUA00600
		COMMON /D/ RAWDAT(2,0:2000),E1(2,0:1000),		DUA00610
		+ARRD(0:1000,5),ARRN(0:1000,5)		DUA00620
				DUA00630
		REAL RYYM(5,5),RYUM(5,5),RUUM(5,5),RUYM(5,5),RUUINV(5,5)		DUA00640
		REAL RYYINV(5,5),DM(5,5),CM(5,5),TRUNRM		DUA00650
				DUA00660
		INTEGER RYYR,RYYC,RUUR,RUUC,RYUR,RYUC,RUYR,RUYC		DUA00670

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INTEGER DR,DC,CR,CC

REAL WKMAT(12,12),X TPO(10,10),Y(2,2),U(1),COEFM(10,10)
INTEGER WKR,WKC,XTR,XTC,COEFR,COEFC,ERR

INTEGER ITERA,CORRLN,YSIZE,USIZE,KTIME,SHFT

DOUBLE PRECISION SEED

* TEMPORATY MATRICES FOR PERFORMING CALCUALTIONS

REAL T1M(5,5),T2M(5,5),T3M(5,5)
INTEGER T1R,T1C,T2R,T2C,T3R,T3C

* BEGIN MAIN PROGRAM
*-----

* READ IN THE SIZE OF THE TEST SYSTEM, THE NUMBER OF ITERATIONS
* TO PERFORM AND THE BEGINNING LAG OF LINEAR PREDICTION OF THE
* AR PARAMETERS

READ(4,*,END=22) YSIZE,USIZE,COEFR,COEFC,ITERA,SHFT

* READ IN THE TRUE VALUES OF THE COEFFICIENTS OF THE TEST SYSTEM

CALL RDMAT(COEFM,COEFR,COEFC)

* INITIALIZE ROW AND COLUMN SIZES OF AS WELL AS OTHER VARIABLES

CORRLN = 500
RUUR = USIZE
RUUC = USIZE
RYYR = YSIZE + 1
RYYC = YSIZE + 1
T3R = YSIZE
T3C = YSIZE
DR = USIZE
DC = 1
CR = YSIZE + 1
CC = 1
XTR = COEFC
XTC = COEFR
SEED = 888.0D1
II = 0
Y(1,1) = 0.0
E1(1,0) = 0.0
DIVISR = TRUNRM(COEFM,COEFR,YSIZE,USIZE)

* ZERO OUT THE CORRELATION MATRICES, THE MA PARAMETER VECTOR AND
* VECTOR OF INPUT DATA

CALL INIT(RYYM,RYYR,RYYC,0.0)
CALL INIT(RUUM,RUUR,RUUC,0.0)
CALL INIT(RYUM,RYYR,RUUC,0.0)
CALL INIT(RUYM,RUUR,RYYC,0.0)

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DUA00680
DUA00690
DUA00700
DUA00710
DUA00720
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DUA00970
DUA00980
DUA00990
DUA01000
DUA01010
DUA01020
DUA01030
DUA01040
DUA01050
DUA01060
DUA01070
DUA01080
DUA01090
DUA01100
DUA01110
DUA01120
DUA01130
DUA01140
DUA01150
DUA01160
DUA01170
DUA01180
DUA01190
DUA01200
DUA01210
DUA01220
DUA01230

```

CALL INIT(DM,DR,DC,0.0)	DUA01240
CALL INIT(X TPO,XTR,XTC,0.0)	DUA01250
* INITIALIZE THE AR PARAMETER VECTOR	DUA01260
CALL INITD(CM,CR,CC,1.0)	DUA01270
CALL PRMAT(CM,CR,CC)	DUA01280
* RUN THE FILTER FOR 2000 TIME STEPS TO GENERATE OUTPUT DATA	DUA01290
*-----	DUA01300
DO 70 KTIME = 0,2000	DUA01310
* GET VALUE FOR U(K). U IS A GAUSSIAN RANDOM VARIABLE.	DUA01320
CALL GGNML (SEED,1,U)	DUA01330
* SHIFT U(K) INTO X VECTOR TO CREATE X(K)	DUA01340
CALL SHIFT(X TPO,XTR,XTC,YSIZE,USIZE,Y(1,1),U(1))	DUA01350
* CALCULATE VALUE OF Y(K)	DUA01360
CALL MULTI(X TPO,XTR,XTC,COEFM,COEFR,COEFC,Y,1,1)	DUA01370
* SAVE THE INPUT AND OUTPUT DATA	DUA01380
RAWDAT(1,KTIME) = Y(1,1)	DUA01390
RAWDAT(2,KTIME) = U(1)	DUA01400
70 CONTINUE	DUA01410
15 FORMAT (2X,I4,2X,F8.5,2X,F8.5)	DUA01420
* CALCULATE THE CORRELATION MATRICES	DUA01430
CALL AUTCOR(1,RYYM,RYYR,RYYC,CORRLN)	DUA01440
CALL AUTCOR(2,RUUM,RUUR,RUUC,CORRLN)	DUA01450
CALL CRSCOR(1,2,RYUM,RYYR,RUUC,CORRLN)	DUA01460
CALL CRSCOR(2,1,RUUM,RUUR,RYYC,CORRLN)	DUA01470
* INVERT THE AUTOCORRELATION MATRICES OF THE OUTPUT AND INPUT DATA	DUA01480
CALL LINV2F(RYYM,RYYR,RYYC,RYYINV,0,WKMAT,ERR)	DUA01490
CALL LINV2F(RUUM,RUUR,RUUC,RUUVINV,0,WKMAT,ERR)	DUA01500
* MULTIPLY THE INVERSE OF THE AUTOCORRELATION MATRICES BY THEIR	DUA01510
* RESPECTIVE CROSSCORRELATION MATRICES	DUA01520
CALL MULTI(RUUVINV,RUUR,RUUC,RUUM,RUUR,RYYC,T1M,T1R,T1C)	DUA01530
CALL MULTI(RYYINV,RYYR,RYYC,RUUM,RYYR,RUUC,T2M,T2R,T2C)	DUA01540
* ESTIMATE THE AR PARAMETERS BY LINEAR PREDICTION	DUA01550
IF (SHFT.GE.1) THEN	DUA01560
CALL CORLA4(DR,CM,CR,CC,T3M,CORRLN,SHFT)	DUA01570
ENDIF	DUA01580
WRITE (3,26) II,DM(1,1),DM(2,1),DM(3,1),DM(4,1),DM(5,1)	DUA01590
WRITE (3,16) II,CM(1,1),CM(2,1),CM(3,1),CM(4,1),CM(5,1)	DUA01600
WRITE (3,*)	DUA01610
CALL SAVE(1,0,II,DM,DR,DC)	DUA01620
	DUA01630
	DUA01640
	DUA01650
	DUA01660
	DUA01670
	DUA01680
	DUA01690
	DUA01700
	DUA01710
	DUA01720
	DUA01730
	DUA01740
	DUA01750
	DUA01760
	DUA01770
	DUA01780
	DUA01790
	DUA01800
	DUA01810
	DUA01820
	DUA01830
	DUA01840
	DUA01850
	DUA01860
	DUA01870
	DUA01880
	DUA01890
	DUA01900
	DUA01910
	DUA01920
	DUA01930
	DUA01940

END	DUA02590
	DUA02600
* *****	DUA02880
SUBROUTINE AUTCOR(IFST,MAT1,M1R,M1C,CORRLN)	DUA02890
* *****	DUA02900
	DUA02910
* THIS SUBROUTINE CALCULATES THE AUTOCORRELATION MATRIX USING	DUA02920
* CORRELATIONS OF SIZE CORRLN	DUA02930
	DUA02940
COMMON /D/ RAWDAT(2,0:2000),E1(2,0:1000),	DUA02950
+ARRD(0:1000,5),ARRN(0:1000,5)	DUA02960
REAL MAT1(M1R,M1C)	DUA02980
INTEGER I,J,K,CORRLN	DUA02990
	DUA03000
CALL INIT(MAT1,M1R,M1C,0.0)	DUA03010
	DUA03020
* CALC CORRELATIONS ALONG THE FIRST ROW OF THE MATRIX. THE	DUA03030
* SHIFT = ABS(NUMBER OF THE COLUMN - 1)	DUA03040
* LENGTH OF CORR = D LENGTH + ABS(1 - THE NUMBER OF THE COLUMN)	DUA03050
	DUA03060
* ONCE CORR HAVE BEEN CALCULATED FOR THE FIRST ROW, THEY CAN	DUA03070
* BE COPIED INTO OTHER ROWS. HORIZ DISTANCE OF THE PARTICULAR	DUA03080
* ELEMENT FROM THE MAIN DIAGONAL DETERMINES WHICH CORR TO	DUA03090
* COPY. THIS DISTANCE IS GIVEN BY ABS(ROWNUMBER - COLUMN	DUA03100
* NUMBER).	DUA03110
	DUA03120
* CORRELATIONS START 200 POINTS FROM THE BEGINNING OF THE	DUA03130
* DATA TO ELIMINATE THE TRANSIENT OF THE TEST SYSTEM.	DUA03140
	DUA03150
DO 90 J = 1,M1C	DUA03160
ENDPT = 200 + CORRLN - ABS(1 - J)	DUA03170
DO 93 K = 200,ENDPT	DUA03180
MAT1(1,J) = MAT1(1,J) + RAWDAT(IFST,K-(1-J))*RAWDAT(IFST,K)	DUA03190
93 CONTINUE	DUA03200
MAT1(1,J) = MAT1(1,J)/(CORRLN + 1 - ABS(1 - J))	DUA03210
90 CONTINUE	DUA03220
	DUA03230
DO 91 I = 2,M1R	DUA03240
DO 92 J = 1,M1C	DUA03250
MAT1(I,J) = MAT1(1,1+ABS(I-J))	DUA03260
92 CONTINUE	DUA03270
91 CONTINUE	DUA03280
	DUA03300
RETURN	DUA03310
END	DUA03320
	DUA03330
* *****	DUA03350
SUBROUTINE COPY(MAT1,M1R,M1C,MAT2,M2R,M2C)	DUA03360
* *****	DUA03370
	DUA03380
* THIS SUBROUTINE COPIES A MATRIX INTO A SECOND MATRIX.	DUA03390
	DUA03400
REAL MAT1(M1R,M1C),MAT2(M2R,M2C)	DUA03410
INTEGER I,J	DUA03420
	DUA03430
DO 90 I = 1,M1R	DUA03440

DO 900 J = 1,M1C	DUA03450
MAT2(I,J) = MAT1(I,J)	DUA03460
900 CONTINUE	DUA03470
90 CONTINUE	DUA03480
M2R = M1R	DUA03500
M2C = M1C	DUA03510
RETURN	DUA03530
END	DUA03540
* *****	DUA03550
SUBROUTINE CRSCOR(IFST,ISND,MAT1,M1R,M1C,CORRLN)	DUA03560
* *****	DUA03570
	DUA03580
	DUA03590
* THIS SUBROUTINE CALCULATES THE CROSSCORRELATION MATRIX USING	DUA03600
* CORRELATIONS OF LENGTH CORRLN	DUA03610
	DUA03620
COMMON /D/ RAWDAT(2,0:2000),E1(2,0:1000),	DUA03630
+ARRD(0:1000,5),ARRN(0:1000,5)	DUA03640
REAL MAT1(M1R,M1C)	DUA03660
INTEGER I,J,K,CORRLN	DUA03670
	DUA03680
CALL INIT(MAT1,M1R,M1C,0.0)	DUA03690
	DUA03700
* FOR CROSS CORRELATION MUST CALC EACH ELEMENT OF THE CORR MATRIX	DUA03710
* SEPARATELY. CORRELATIONS START 200 POINTS FROM THE BEGINNING	DUA03720
* OF THE DATA TO ELIMINATE THE TRANSIENT OF THE TEST SYSTEM.	DUA03730
	DUA03740
DO 94 I = 1,M1R	DUA03760
DO 95 J = 1,M1C	DUA03770
ENDPT = 200 + CORRLN - ABS(I - J)	DUA03780
IF (J.GE.I) THEN	DUA03790
DO 96 K = 200,ENDPT	DUA03800
MAT1(I,J) = MAT1(I,J) + RAWDAT(IFST,K-(I-J))	DUA03810
96 +*RAWDAT(ISND,K)	DUA03820
CONTINUE	DUA03830
ELSE	DUA03840
DO 97 K = 200,ENDPT	DUA03850
MAT1(I,J) = MAT1(I,J) + RAWDAT(IFST,K)*	DUA03860
97 +*RAWDAT(ISND,K+(I-J))	DUA03870
CONTINUE	DUA03880
ENDIF	DUA03890
MAT1(I,J) = MAT1(I,J)/(CORRLN + 1 - ABS(I-J))	DUA03900
95 CONTINUE	DUA03910
94 CONTINUE	DUA03920
RETURN	DUA03950
END	DUA03960
	DUA03970
* *****	DUA03980
SUBROUTINE CORLA4(ISIZE,MAT2,M2R,M2C,MAT3,CORRLN,SHIFTT)	DUA03990
* *****	DUA04000
	DUA04010
* THIS SUBROUTINE CALCULATES THE CORRELATION MATRIX	DUA04020
* AND THE CORRELATION VECTOR USED FOR LINEAR PREDICTION OF THE	DUA04030
* AR PARAMETERS. IT THEN CALCULATES THE INITIAL ESTIMATE OF THE	DUA04040
* AR PARAMETERS AND PASSES THEM BACK TO THE MAIN PROGRAM IN MAT2.	DUA04050
	DUA04060

COMMON /D/ RAWDAT(2,0:2000),E1(2,0:1000),	DUA04070
+ARRD(0:1000,5),ARRN(0:1000,5)	DUA04080
REAL MAT2(M2R,M2C),MAT3(M2R-1,M2R-1)	DUA04100
REAL T2M(5,1),T3M(5,1),T4M(5,5),WKMAT(9,9)	DUA04110
INTEGER ERR,T1R,T1C,T2R,T2C,T3R,T3C,ISIZE,SHIFTT,CORRLN	DUA04130
	DUA04140
* GENERATE THE FIRST ROW OF THE RYY MATRIX.	DUA04150
* SHIFTS ARE GREATER THAN THE ORDER OF THE	DUA04160
* NUMERATOR.	DUA04170
	DUA04180
M3R = M2R-1	DUA04190
M3C = M3R	DUA04200
CALL INIT(MAT3,M3R,M3C,0.0)	DUA04210
	DUA04220
DO 90 J = 1,M3C	DUA04230
ENDPT = 200 + CORRLN - SHIFTT	DUA04240
DO 91 K = 200,ENDPT	DUA04250
MAT3(1,J) = MAT3(1,J) + RAWDAT(1,K+SHIFTT)*RAWDAT(1,K)	DUA04260
91 CONTINUE	DUA04270
MAT3(1,J) = MAT3(1,J)/(CORRLN-SHIFTT+1)	DUA04280
SHIFTT = SHIFTT + 1	DUA04290
90 CONTINUE	DUA04300
	DUA04310
* COPY ELEMENTS FROM THE FIRST ROW INTO OTHER LOCATIONS	DUA04320
	DUA04330
DO 92 I = 2,M3R	DUA04340
DO 93 J = 1,M3C	DUA04350
MAT3(I,J) = MAT3(1,1+ABS(I-J))	DUA04360
93 CONTINUE	DUA04370
92 CONTINUE	DUA04380
	DUA04390
* GENERATE THE RYY VECTOR BY COPYING ELEMENTS OF THE RYY MATRIX	DUA04400
	DUA04410
T2R = M3C	DUA04420
T2C = 1	DUA04430
CALL FILL(1,T2R-1,1,1,T2M,T2R,1,2,1,MAT3,M3R,M3C)	DUA04440
	DUA04450
* GENERATE THE LAST ELEMENT IN THE RYY CORRELATION VECTOR.	DUA04460
	DUA04470
FINELE = 0.0	DUA04480
ENDPT = 200 + CORRLN - SHIFTT	DUA04490
DO 94 K = 200,ENDPT	DUA04500
FINELE = FINELE + RAWDAT(1,K+SHIFTT)*RAWDAT(1,K)	DUA04510
94 CONTINUE	DUA04520
FINELE = FINELE/(CORRLN+1-SHIFTT)	DUA04530
	DUA04540
* COPY THE FINAL ELEMENT INTO THE VECTOR	DUA04550
T2M(T2R,1) = FINELE	DUA04570
	DUA04580
* CALCULATE THE INITIAL ESTIMATE OF THE AR PARAMETERS	DUA04630
	DUA04640
CALL LINV2F(MAT3,M3R,M3C,T4M,0,WKMAT,ERR)	DUA04650
CALL MULTI(T4M,M3R,M3C,T2M,T2R,T2C,T3M,T3R,T3C)	DUA04670
	DUA04690
* COPY THE AR PARAMETERS INTO THE RETURN ARGUMENT	DUA04700
	DUA04710

	MAT2(1,1) = 1.0	DUA04720
	DO 95 L = 1,3	DUA04730
	MAT2(L + 1,1) = T3M(L,1)	DUA04740
*	MAT2(L,1) = T3M(L-1,1)	DUA04750
*	WRITE (3,*) MAT2(L,1)	DUA04760
95	CONTINUE	DUA04770
		DUA04800
	RETURN	DUA04810
	END	DUA04820
		DUA04830
*	*****	DUA04840
	SUBROUTINE ERROR(MAT1,M1R,M1C,MAT2,M2R,M2C,ITNUM)	DUA04850
*	*****	DUA04860
		DUA04870
*	THIS SUBROUTINE CALCULATES THE STOPPING PARAMETER.	DUA04880
		DUA04890
	COMMON /D/ RAWDAT(2,0:2000),E1(2,0:1000),	DUA04900
	+ARRD(0:1000,5),ARRN(0:1000,5)	DUA04910
	REAL MAT1(M1R,M1C),MAT2(M2R,M2C)	DUA04930
	INTEGER I,J,K	DUA04940
		DUA04950
	ERVAL = 0.0	DUA04960
	XVAL = 0.0	DUA04970
	ZVAL = 0.0	DUA04980
		DUA04990
	DO 90 I = 400,450	DUA05000
	DO 91 J = M1R,1,-1	DUA05010
	XVAL = XVAL + MAT1(J,1)*RAWDAT(1,I+M1R-J)	DUA05020
91	CONTINUE	DUA05030
	DO 92 K = M2R,1,-1	DUA05040
	ZVAL = ZVAL + MAT2(K,1)*RAWDAT(2,I+M2R-K)	DUA05050
92	CONTINUE	DUA05060
		DUA05070
	ERVAL = ERVAL + (XVAL-ZVAL)**2	DUA05080
	XVAL = 0.0	DUA05090
	ZVAL = 0.0	DUA05100
90	CONTINUE	DUA05110
		DUA05120
	E1(1,ITNUM) = ERVAL/51	DUA05130
		DUA05140
	RETURN	DUA05150
	END	DUA05160
		DUA05170
*	*****	DUA05190
	SUBROUTINE ERR2(MAT1,M1R,MAT2,M2R,MAT3,M3R,ITNUM,	DUA05200
	+YSZ,USZ,DIVISR)	DUA05210
*	*****	DUA05220
		DUA05230
*	THIS SUBROUTINE CALCUALTES THE COEFFICIENT ERROR.	DUA05240
		DUA05250
	COMMON /D/ RAWDAT(2,0:2000),E1(2,0:1000),	DUA05260
	+ARRD(0:1000,5),ARRN(0:1000,5)	DUA05270
	REAL MAT1(M1R,1),MAT2(M2R,1),MAT3(M3R,1)	DUA05290
	INTEGER I,YSZ,USZ	DUA05300
		DUA05320
	ERRVAL = (1 - MAT2(1,1))**2	DUA05330

	DO 90 I = 1,YSZ	DUA05340
	ERRVAL = ERRVAL + (MAT1(I,1) + MAT2(I+1,1))**2	DUA05350
90	CONTINUE	DUA05360
		DUA05370
	DO 92 I = 1,USZ	DUA05380
	ERRVAL = ERRVAL + (MAT1(I+YSZ,1) - MAT3(I,1))**2	DUA05390
92	CONTINUE	DUA05400
		DUA05410
	E1(2,ITNUM) = SQRT(ERRVAL)/DIVISR	DUA05420
		DUA05430
	RETURN	DUA05440
	END	DUA05450
		DUA05460
*	*****	DUA05480
*	SUBROUTINE FILL(I,J,K,L,MAT1,M1R,M1C,R2,C2,MAT2,M2R,M2C)	DUA05490
*	*****	DUA05500
		DUA05510
		DUA05520
*	THIS ROUTINE FILLS MAT1 FROM MAT2. POSITIONS	DUA05530
*	IN MAT1 FROM (I,K) TO (J,L) ARE FILLED WITH AN EQUAL NUMBER	DUA05540
*	OF ELEMENTS FROM MAT2 STARTING AT POSITION (R2,C2).	DUA05550
		DUA05560
	REAL MAT1(M1R,M1C),MAT2(M2R,M2C)	DUA05570
	INTEGER ROW,COL,R2,C2,C22	DUA05590
		DUA05600
	C22 = C2	DUA05610
		DUA05620
	DO 90 ROW = I,J	DUA05640
	DO 91 COL = K,L	DUA05650
	MAT1(ROW,COL) = MAT2(R2,C2)	DUA05660
	C2 = C2 + 1	DUA05670
91	CONTINUE	DUA05680
	R2 = R2 + 1	DUA05690
	C2 = C22	DUA05700
90	CONTINUE	DUA05710
		DUA05720
	RETURN	DUA05730
	END	DUA05740
		DUA05750
*	*****	DUA07000
*	SUBROUTINE LIM2(EMAX,ESTP,CEMAX,CESTP,ITERA)	DUA07010
*	*****	DUA07020
		DUA07030
*	ROUTINE CALCULATES THE LIMITS FOR THE GRAPH OF THE STOPPING	DUA07040
*	PARAMETER AND THE COEFFICIENT ERROR.	DUA07050
*	STOPPING PARAMETER LIMITS ARE RETURNED IN EMAX AND ESTP.	DUA07060
*	COEFFICIENT ERROR LIMITS ARE RETURNED IN CEMAX AND CESTP.	DUA07070
		DUA07080
	COMMON /D/ RAWDAT(2,0:2000),E1(2,0:1000),	DUA07090
	+ARRD(0:1000,5),ARRN(0:1000,5)	DUA07100
	REAL EMAX,ESTP	DUA07120
	INTEGER ITERA	DUA07130
		DUA07140
	EMAX = 0.0	DUA07150
	DO 90 I = 0,ITERA	DUA07160
	IF (E1(1,I).GT.EMAX) THEN	DUA07180

	EMAX = E1(1,I)	DUA07190
	ENDIF	DUA07200
90	CONTINUE	DUA07220
	EMAX = 1.25 * EMAX	DUA07230
	ESTP = EMAX/5	DUA07240
	CEMAX = 0.0	DUA07280
	DO 91 I = 0,ITERA	DUA07290
	IF (E1(2,I).GT.CEMAX) THEN	DUA07310
	CEMAX = E1(2,I)	DUA07320
	ENDIF	DUA07330
91	CONTINUE	DUA07350
	CEMAX = 1.25 * CEMAX	DUA07360
	CESTP = CEMAX/5	DUA07370
	RETURN	DUA07380
	END	DUA07390
*	*****	DUA07400
*	SUBROUTINE PLOT1(ITERA,ICURVN,ICURVD,MAT1)	DUA07670
*	*****	DUA07680
		DUA07690
		DUA07700
*	THIS ROUTINE GENERATES SEPARATE PLOTS OF THE MA	DUA07710
*	AND AR PARAMETERS. IT THEN REPLOTS THE THESE CURVES ALONG	DUA07720
*	WITH THE STOPPING PARAMETER. FINALLY IT PLOTS THE STOPPING	DUA07730
*	PARAMETER AND THE COEFFICIENT ERROR ON THE SAME GRAPH.	DUA07740
		DUA07750
	COMMON /D/ RAWDAT(2,0:2000),E1(2,0:1000),	DUA07760
	+ARRD(0:1000,5),ARRN(0:1000,5)	DUA07770
	REAL X(0:1000),Y(0:1000),MAT1(10,10)	DUA07780
	REAL STP,RNMIN,RNSTEP,RNMAX,RITERA	DUA07790
	INTEGER I,J,IIR,IIC,VAL,ITERA,ICURV	DUA07800
		DUA07810
	CALL LIMITS(ICURVN,ICURVD,DMAX,DMIN,DSTEP,	DUA07820
	+NMAX,NMIN,NSTEP,ITERA)	DUA07830
	CALL LIM2(EMAX,ESTP,CEMAX,CESTP,ITERA)	DUA07840
		DUA07870
*	GENERATE THE ITERATION NUMBER	DUA07880
		DUA07890
	DO 90 I = 0,ITERA	DUA07900
	X(I) = I	DUA07910
	Y(I) = 0.0	DUA07920
90	CONTINUE	DUA07930
		DUA07940
*	CALCULATE X AXIS LABELING INTERVAL	DUA07950
	STP = ITER / 10.	DUA07970
		DUA07980
*	SET THE DEVICE CALLS FOR ALL OF THE PLOTS	DUA07990
		DUA08000
	CALL SHERPA('MCGRAF ','A',3)	DUA08030
	CALL RESET('ALL')	DUA08050
		DUA08060
*	SECTION 1	DUA08070
*	THIS SECTION GRAPHS THE NUMERATOR AND DENOMINATOR	DUA08080
*	PARAMETERS ON SEPARATE GRAPHS ON THE SAME PAGE.	DUA08090

* SET UP THE PLOT FOR THE NUMERATOR COEFF

```
CALL PAGE(8.5,11.0)
CALL HEIGHT(0.14)
CALL HWROT('AUTO')
CALL XINTAX
CALL PHYSOR(1.5,6.0)
CALL AREA2D(5.0,3.5)
CALL COMPLX
CALL YAXANG(0)
CALL XNAME('ITERATIONS$',100)
CALL YNAME('PARAMETER VALUES$',100)
CALL MESSAG('(A)$',100,2.4,-0.8)
CALL THKFRM(0.03)
CALL FRAME
CALL GRAF(0.,STP,ITERA,NMIN,NSTEP,NMAX)
```

* PLOT THE NUMERATOR PARAMETERS

```
DO 93 J = 1,ICURVN
  DO 94 I = 0,ITERA
    Y(I) = ARRN(I,J)
94  CONTINUE
    CALL CURVE(X,Y,ITERA,0)
93  CONTINUE
```

* PLOT DASHED LINES FOR THE TRUE VALUE OF THE PARAMETERS

```
CALL DASH
DO 97 K = ICURVD,ICURVD+ICURVN-1
  DO 98 J = 0,ITERA
    Y(J) = MAT1(K,1)
98  CONTINUE
    CALL CURVE(X,Y,ITERA,0)
97  CONTINUE
    CALL ENDGR(0)
```

* SET UP THE PLOT FOR THE DENOMINATOR PARAMETERS

```
CALL RESET('DASH')
CALL PHYSOR(1.5,1.5)
CALL AREA2D(5.0,3.5)
CALL XNAME('ITERATIONS$',100)
CALL YNAME('PARAMETER VALUES$',100)
CALL MESSAG('(B)$',100,2.4,-0.8)
CALL THKFRM(0.03)
CALL FRAME
CALL GRAF(0.,STP,ITERA,DMIN,DSTEP,DMAX)
```

* PLOT THE DENOMINATOR PARAMETERS

```
DO 95 J = 1,ICURVD
  DO 96 I = 0,ITERA
    Y(I) = ARRD(I,J)
96  CONTINUE
```

DUA08100
DUA08110
DUA08120
DUA08130
DUA08140
DUA08150
DUA08160
DUA08170
DUA08200
DUA08210
DUA08240
DUA08250
DUA08260
DUA08270
DUA08280
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DUA08750
DUA08760

95	CALL CURVE(X,Y,ITERA,0)	DUA08770
	CONTINUE	DUA08780
		DUA08790
	* PLOT DASHED LINES FOR THE TRUE VALUES OF THE DENOM PARAMETERS	DUA08800
	CALL DASH	DUA08810
	DO 99 K = 1,ICURVD-1	DUA08820
	DO 100 J = 0,ITERA	DUA08830
	Y(J) = -MAT1(K,1)	DUA08840
100	CONTINUE	DUA08850
	CALL CURVE(X,Y,ITERA,0)	DUA08860
99	CONTINUE	DUA08870
		DUA08880
	DO 105 J = 0,ITERA	DUA08890
	Y(J) = 1.0	DUA08900
105	CONTINUE	DUA08910
	CALL CURVE(X,Y,ITERA,0)	DUA08920
	CALL ENDPL(0)	DUA08930
		DUA08940
		DUA08950
	* SECTION 2	DUA08960
	* THIS SECTION PUTS THE STOPPING PARAMETER ON THE	DUA08970
	* GRAPHS OF THE NUMERATOR AND DENOMINATOR PARAMETERS.	DUA08980
		DUA08990
	* SET UP THE PLOT FOR THE NUMERATOR PARAMETERS	DUA09010
	CALL RESET('DASH')	DUA09020
	CALL HWROT('AUTO')	DUA09030
	CALL XINTAX	DUA09040
	CALL PHYSOR(1.5,6.0)	DUA09050
	CALL AREA2D(5.0,3.5)	DUA09060
	CALL COMPLX	DUA09090
	CALL YAXANG(0)	DUA09100
	CALL XNAME('ITERATIONS\$',100)	DUA09130
	CALL YNAME('PARAMETER VALUES\$',100)	DUA09140
	CALL MESSAG('(A)\$',100,2.4,-0.8)	DUA09150
	CALL THKFRM(0.03)	DUA09160
	CALL FRAME	DUA09170
	CALL GRAF(0.,STP,ITERA,NMIN,NSTEP,NMAX)	DUA09180
		DUA09190
		DUA09210
	* PLOT THE NUMERATOR PARAMETERS	DUA09220
	DO 200 J = 1,ICURVN	DUA09230
	DO 201 I = 0,ITERA	DUA09240
	Y(I) = ARRN(I,J)	DUA09250
201	CONTINUE	DUA09260
	CALL CURVE(X,Y,ITERA,0)	DUA09270
200	CONTINUE	DUA09280
		DUA09290
		DUA09300
	* PLOT DASHED LINES FOR THE TRUE VALUES OF THE PARAMETERS	DUA09310
	CALL DASH	DUA09320
	DO 202 K = ICURVD,ICURVD+ICURVN-1	DUA09330
	DO 203 J = 0,ITERA	DUA09340
	Y(J) = MAT1(K,1)	DUA09350
203	CONTINUE	DUA09360
		DUA09370

```

                CALL CURVE(X,Y,ITERA,0)
202    CONTINUE

*   PLOT THE STOPPING PARAMETER ON THE SAME GRAPH

        CALL DOT
        CALL YGRAXS(0.0,ESTP,EMAX,3.5,'STOPPING PARAMETERS$',
+-100,5.0,0.0)

        DO 204 J = 0,ITERA
            Y(J) = E1(1,J)
204    CONTINUE
        CALL CURVE(X,Y,ITERA,0)
        CALL ENDGR(0)

*   SET UP THE PLOT FOR THE DENOMINATOR PARAMETERS

        CALL RESET('DOT')
        CALL PHYSOR(1.5,1.5)
        CALL AREA2D(5.0,3.5)
        CALL XNAME('ITERATIONS$',100)
        CALL YNAME('PARAMETER VALUES$',100)
        CALL MESSAG('(B)$',100,2.4,-0.8)
        CALL THKFRM(0.03)
        CALL FRAME
        CALL GRAF(0.,STP,ITERA,DMIN,DSTEP,DMAX)

*   PLOT THE DENOMINATOR PARAMETERS

        DO 205 J = 1,ICURVD
            DO 206 I = 0,ITERA
                Y(I) = ARRD(I,J)
206    CONTINUE
            CALL CURVE(X,Y,ITERA,0)
205    CONTINUE

*   PLOT DASHED LINES FOR THE TRUE VALUES OF THE PARAMETERS

        CALL DASH
        DO 207 K = 1,ICURVD-1
            DO 208 J = 0,ITERA
                Y(J) = -MAT1(K,1)
208    CONTINUE
            CALL CURVE(X,Y,ITERA,0)
207    CONTINUE

        DO 209 J = 0,ITERA
            Y(J) = 1.0
209    CONTINUE
        CALL CURVE(X,Y,ITERA,0)

*   PLOT THE STOPPING PARAMETER ON THE SAME GRAPH

        CALL DOT

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DUA09380
DUA09390
DUA09400
DUA09410
DUA09420
DUA09430
DUA09440
DUA09450
DUA09460
DUA09470
DUA09480
DUA09490
DUA09500
DUA09510
DUA09520
DUA09530
DUA09540
DUA09550
DUA09560
DUA09570
DUA09580
DUA09590
DUA09610
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DUA09630
DUA09640
DUA09650
DUA09660
DUA09680
DUA09690
DUA09700
DUA09710
DUA09720
DUA09730
DUA09740
DUA09750
DUA09760
DUA09770
DUA09780
DUA09790
DUA09800
DUA09810
DUA09820
DUA09830
DUA09840
DUA09850
DUA09860
DUA09870
DUA09880
DUA09890
DUA09900
DUA09910
DUA09920
DUA09930
DUA09940
DUA09950

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      CALL YGRAXS(0.0,ESTP,EMAX,3.5,'STOPPING PARAMETERS',
+-100,5.0,0.0)

      DO 210 J = 0,ITERA
        Y(J) = E1(1,J)
210    CONTINUE
      CALL CURVE(X,Y,ITERA,0)
      CALL ENDPL(0)

* SECTION 3
* THIS SECTION PLOTS THE STOPPING PARAMETER AND THE COEFFICIENT
* ERROR ON THE SAME GRAPH.

* SETUP THE PLOT FOR THE STOPPING PARAMETER

      CALL DOT
      CALL HWROT('AUTO')
      CALL PHYSOR(1.5,6.0)
      CALL AREA2D(5.0,3.5)
      CALL XNAME('ITERATIONS$',100)
      CALL YNAME('STOPPING PARAMETER$',100)
      CALL THKFRM(0.03)
      CALL FRAME
      CALL GRAF(0.,STP,ITERA,0.,ESTP,EMAX)

      DO 306 J = 0,ITERA
        Y(J) = E1(1,J)
306    CONTINUE
      CALL CURVE(X,Y,ITERA,0)

* PLOT THE COEFFICIENT ERROR ON THE SAME GRAPH

      CALL CHNDOT
      CALL YGRAXS(0.0,CESTP,CEMAX,3.5,'COEFFICIENT ERROR$',
+-100,5.0,0.0)

      DO 307 J = 0,ITERA
        Y(J) = E1(2,J)
307    CONTINUE
      CALL CURVE(X,Y,ITERA,0)
      CALL ENDPL(0)
      CALL DONEPL
      RETURN
      END

* *****
* SUBROUTINE SAVE(VAL,M,K,MAT1,M1R,M1C)
* *****

* ROUTINE SAVES PARAMETER ESTIMATES IN EITHER ARRD OR ARRN
* DEPENDING UPON THE VALUE OF VAL.

      COMMON /D/ RAWDAT(2,0:2000),E1(2,0:1000),
+ARRD(0:1000,5),ARRN(0:1000,5)

```

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DUA09960
DUA09970
DUA09980
DUA09990
DUA10000
DUA10010
DUA10020
DUA10030
DUA10040
DUA10050
DUA10060
DUA10070
DUA10080
DUA10090
DUA10100
DUA10110
DUA10120
DUA10130
DUA10140
DUA10150
DUA10160
DUA10180
DUA10190
DUA10200
DUA10220
DUA10230
DUA10240
DUA10250
DUA10260
DUA10270
DUA10280
DUA10290
DUA10300
DUA10310
DUA10320
DUA10330
DUA10340
DUA10350
DUA10360
DUA10370
DUA10380
DUA10390
DUA10400
DUA10410
DUA10420
DUA10430
DUA10440
DUA10860
DUA10870
DUA10880
DUA10890
DUA10900
DUA10910
DUA10920
DUA10930
DUA10940

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REAL MAT1(M1R,M1C)	DUA10960
INTEGER I,J,K,M,VAL	DUA10970
DO 90 I = 1,M1R	DUA10980
DO 900 J = 1,M1C	DUA10990
IF (VAL.EQ.1) THEN	DUA11000
ARRN(K,I) = MAT1(I,J)	DUA11010
ELSEIF (VAL.EQ.2) THEN	DUA11020
ARRD(K,I) = MAT1(I,J)	DUA11030
ENDIF	DUA11040
900 CONTINUE	DUA11050
90 CONTINUE	DUA11060
	DUA11070
	DUA11080
RETURN	DUA11090
END	DUA11100

C. SUBPROGRAMS COMMON TO BOTH SYSTEM IDENTIFICATION ALGORITHMS SUB00010

	SUB00020
* *****	SUB00040
SUBROUTINE ADD (MAT1,IR1,IC1,MAT2,IR2,IC2,RMAT,IRR,IRC)	SUB00050
* *****	SUB00060
	SUB00070
* THIS SUBROUTINE ADDS TWO EQUAL SIZE MATRICIES AND PUTS THE RESULT	SUB00080
* IN A THIRD MATRIX.	SUB00090
	SUB00100
REAL MAT1(IR1,IC1),MAT2(IR2,IC2),RMAT(IR1,IC1)	SUB00130
INTEGER I,J,IRR,IRC	SUB00140
	SUB00160
DO 92 I=1,IR1	SUB00170
DO 920 J=1,IC1	SUB00180
RMAT(I,J) = MAT1(I,J) + MAT2(I,J)	SUB00190
920 CONTINUE	SUB00200
92 CONTINUE	SUB00210
IRR = IR1	SUB00220
IRC = IC1	SUB00230
RETURN	SUB00240
END	SUB00250
	SUB00260
* *****	SUB00280
SUBROUTINE INIT(MAT1,M1R,M1C,INITVL)	SUB00290
* *****	SUB00300
	SUB00310
* THIS SUBROUTINE INITIALIZES A MATRIX TO INITVL	SUB00320
	SUB00330
REAL MAT1(M1R,M1C),INITVL	SUB00340
INTEGER I,J	SUB00350
	SUB00360
DO 94 I=1,M1R	SUB00380
DO 95 J=1,M1C	SUB00390
MAT1(I,J)=INITVL	SUB00400
95 CONTINUE	SUB00410
94 CONTINUE	SUB00420
RETURN	SUB00430

END	SUB00440
	SUB00450
* *****	SUB00470
SUBROUTINE INITD(MAT1,M1R,M1C,INITVL)	SUB00480
* *****	SUB00490
	SUB00500
* THIS SUBROUTINE INITIALIZES A MATRIX TO AS A DIAGONAL MATRIX	SUB00510
* WHOSE DIAGONAL ELEMENTS EQUAL INITVL.	SUB00520
	SUB00530
REAL MAT1(M1R,M1C),INITVL	SUB00540
INTEGER I,J	SUB00550
	SUB00570
DO 94 I=1,M1R	SUB00580
DO 95 J=1,M1C	SUB00590
IF (I.EQ.J) THEN	SUB00600
MAT1(I,J)=INITVL	SUB00610
ELSE	SUB00620
MAT1(I,J)=0.0	SUB00630
ENDIF	SUB00640
95 CONTINUE	SUB00650
94 CONTINUE	SUB00660
RETURN	SUB00670
END	SUB00680
	SUB00690
* *****	SUB00710
SUBROUTINE LIMITS(NSZ,DSZ,DMAX,DMIN,DSTEP,NMAX,NMIN,NSTEP,ITERA)	SUB00720
* *****	SUB00730
	SUB00740
* ROUTINE CALCULATES THE LIMITS FOR THE GRAPHS	SUB00750
* CALCULATES DENOMINATOR AND NUMERATOR LIMITS SEPARATELY	SUB00760
* IN PREPARATION FOR MAKING TWO GRAPHS	SUB00770
	SUB00780
COMMON /D/ RAWDAT(2,0:2000),E1(2,0:1000),	SUB00790
+ARRD(0:1000,5),ARRN(0:1000,5)	SUB00800
REAL DMAX,DMIN,DSTEP,NMAX,NMIN,NSTEP	SUB00820
INTEGER DSZ,NSZ	SUB00830
	SUB00840
* CALCULATE THE DENOMINATOR LIMITS	SUB00850
	SUB00860
DMAX = 1.0	SUB00870
DMIN = 0.0	SUB00880
	SUB00890
DO 90 I = 1,DSZ	SUB00900
DO 91 J = 0,ITERA	SUB00910
IF ((ARRD(J,I)).GT.DMAX) THEN	SUB00920
DMAX = ARRD(J,I)	SUB00930
ENDIF	SUB00940
IF ((ARRD(J,I)).LT.DMIN) THEN	SUB00950
DMIN = ARRD(J,I)	SUB00960
ENDIF	SUB00970
91 CONTINUE	SUB00980
90 CONTINUE	SUB00990
	SUB01000
IF (DMAX.GT.0) THEN	SUB01010
DMAX = 1.25 * DMAX	SUB01020
ELSE	SUB01030

DMAX = 0.0	SUB01040
ENDIF	SUB01050
IF (DMIN.GT.0) THEN	SUB01060
DMIN = 0.0	SUB01070
ELSE	SUB01080
DMIN = 1.25 * DMIN	SUB01090
ENDIF	SUB01100
DSTEP = (DMAX - DMIN)/5	SUB01110
	SUB01130
	SUB01140
* CALCULATE THE NUMERATOR LIMITS	SUB01150
	SUB01160
NMAX = 0.0	SUB01170
NMIN = 0.0	SUB01180
DO 92 I = 1,NSZ	SUB01190
DO 93 J = 0,ITERA	SUB01200
IF (ARRN(J,I).GT.NMAX) THEN	SUB01210
NMAX = ARRN(J,I)	SUB01220
ENDIF	SUB01230
	SUB01240
IF (ARRN(J,I).LT.NMIN) THEN	SUB01250
NMIN = ARRN(J,I)	SUB01260
ENDIF	SUB01270
93 CONTINUE	SUB01280
92 CONTINUE	SUB01290
	SUB01300
IF (NMAX.GT.0) THEN	SUB01310
NMAX = 1.25 * NMAX	SUB01320
ELSE	SUB01330
NMAX = 0.0	SUB01340
ENDIF	SUB01350
	SUB01360
IF (NMIN.GT.0) THEN	SUB01370
NMIN = 0.0	SUB01380
ELSE	SUB01390
NMIN = 1.25 * NMIN	SUB01400
ENDIF	SUB01410
NSTEP = ABS(NMAX - NMIN)/5	SUB01430
	SUB01440
RETURN	SUB01450
END	SUB01460
	SUB01470
* *****	SUB01490
SUBROUTINE MULTI (MAT1,M1R,M1C,MAT2,M2R,M2C,RMAT,M3R,M3C)	SUB01500
* *****	SUB01510
	SUB01520
* ROUTINE MULTIPLIES TWO MATRICES AND PUT THE RESULT IN A	SUB01530
* THIRD MATRIX.	SUB01540
	SUB01550
REAL MAT1(M1R,M1C),MAT2(M2R,M2C),RMAT(M1R,M2C)	SUB01580
INTEGER I,J,K,IRR,IRC	SUB01590
	SUB01600
CALL INIT(RMAT,M1R,M2C,0.0)	SUB01610
	SUB01620
DO 91 I=1,M1R	SUB01630
DO 910 J=1,M2C	SUB01640

	DO 9100 K=1,M1C	SUB01650
	RMAT(I,J)=RMAT(I,J) +MAT1(I,K)*MAT2(K,J)	SUB01660
9100	CONTINUE	SUB01670
910	CONTINUE	SUB01680
91	CONTINUE	SUB01690
	M3R = M1R	SUB01700
	M3C = M2C	SUB01710
	RETURN	SUB01720
	END	SUB01730
		SUB01740
*	*****	IVA04910
*	SUBROUTINE PRMAT(MAT1,I1R,I1C)	IVA04920
*	*****	IVA04930
*	SUBROUTINE PRINTS A MATRIX OUT TO THE FILE DEFINED	
*	AS UNIT 3	
	REAL MAT1(10,10)	IVA04970
	INTEGER I,J	IVA04980
		IVA04990
	DO 92 I = 1,I1R	IVA05010
	WRITE(3,302) (MAT1(I,J),J = 1,I1C)	IVA05020
302	FORMAT (7(2X,F8.5))	IVA05030
92	CONTINUE	IVA05040
	RETURN	IVA05050
	END	IVA05060
		IVA05070
*	*****	SUB01760
*	SUBROUTINE RDMAT(MAT1,M1R,M1C)	SUB01770
*	*****	SUB01780
*	ROUTINE READS A MATRIX FROM FILE SPECIFIED AS UNIT 4.	SUB01790
	REAL MAT1(M1R,M1C)	SUB01800
	INTEGER I,J	SUB01810
		SUB01840
		SUB01850
*	READ IN MATRIX	SUB01860
		SUB01870
		SUB01880
	DO 92 I = 1,M1R	SUB01890
	READ (4,*) (MAT1(I,J),J=1,M1C)	SUB01900
C301	FORMAT(10F3.1)	SUB01910
92	CONTINUE	SUB01920
	RETURN	SUB01930
	END	SUB01940
		SUB01950
*	*****	SUB01970
*	SUBROUTINE SHIFT(MAT1,M1R,M1C,DSIZE,NSIZE,OUTDAT,INDAT)	SUB01980
*	*****	SUB01990
*		SUB02000
*	ROUTINE SHIFTS NEW INPUT AND OUTPUT VALUES INTO DATA VECTOR	SUB02010
*	OF THE TEST SYSTEM. THE OLDEST VALUES ARE LOST TO MAKE	SUB02020
*	ROOM FOR THE NEW VALUES.	SUB02030
		SUB02060
	REAL MAT1(M1R,M1C),OUTDAT(1),INDAT(1)	SUB02070
	INTEGER J,DSIZE,NSIZE,NSTART	SUB02080
		SUB02090

	NSTART = DSIZE + 1	SUB02100
	DO 92 J = DSIZE,2,-1	SUB02110
	MAT1(1,J) = MAT1(1,J-1)	SUB02120
92	CONTINUE	SUB02130
	MAT1(1,1) = OUTDAT(1)	SUB02140
		SUB02150
	DO 93 J = M1C,NSTART+1,-1	SUB02160
	MAT1(1,J) = MAT1(1,J-1)	SUB02170
93	CONTINUE	SUB02180
	MAT1(1,NSTART) = INDAT(1)	SUB02190
	WRITE(12,19) (MAT1(1,J),J=1,M1C)	SUB02200
19	FORMAT (7(1X,F8.4))	SUB02210
		SUB02220
	RETURN	SUB02230
	END	SUB02240
		SUB02260
*	*****	SUB02270
	SUBROUTINE SMULTI (CONST,MAT1,M1R,M1C)	SUB02280
*	*****	SUB02290
		SUB02300
*	ROUTINE MULTIPLIES A MATRIX BY A SCALAR.	SUB02310
		SUB02320
	REAL MAT1(M1R,M1C),CONST	SUB02350
	INTEGER I,J	SUB02370
		SUB02380
	DO 93 I=1,M1R	SUB02390
	DO 930 J=1,M1C	SUB02400
	MAT1(I,J) = MAT1(I,J) * CONST	SUB02410
930	CONTINUE	SUB02420
93	CONTINUE	SUB02430
		SUB02440
	RETURN	SUB02450
	END	SUB02460

SUB02480

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